

1915

N.W.F.
So Dir

T - 18

TRANSIT BOOK

14.113.0117

O.K.

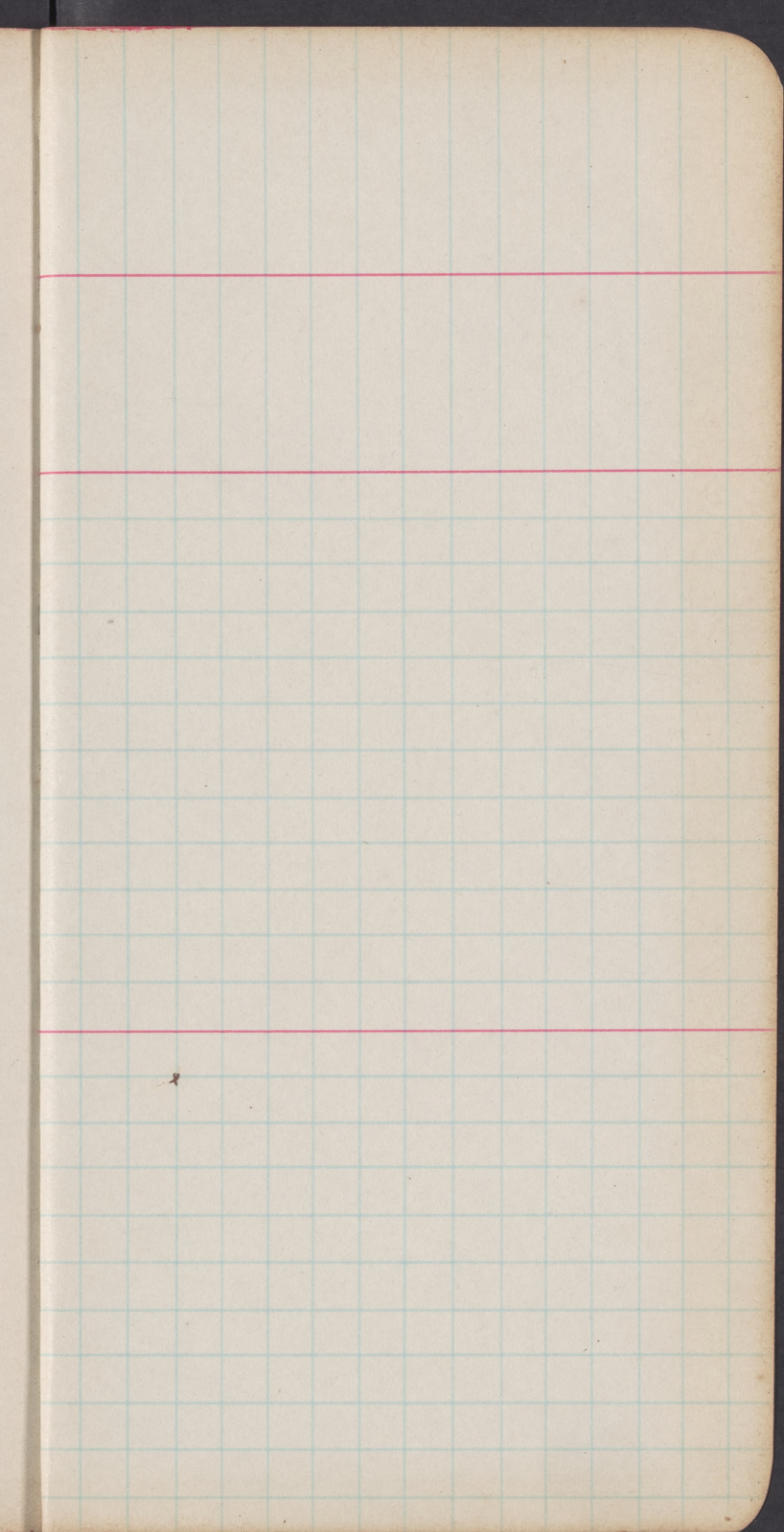


$$\begin{array}{r}
 156.25 \\
 168.15 \\
 \hline
 324.40
 \end{array}$$

$$\begin{array}{r}
 68.55 \\
 31.85 \\
 \hline
 48 \quad \checkmark \\
 0
 \end{array}$$

$$\begin{array}{r}
 45. \\
 25.03 \\
 \hline
 70.03
 \end{array}$$

$$\begin{array}{r}
 16 \\
 3 \\
 \hline
 4.8. \\
 22.4. \\
 \hline
 192.2' \\
 192 \\
 96 \\
 \hline
 117.1.2 \quad | \\
 60 \\
 \hline
 1057.1 \\
 1038 \\
 \hline
 12'3.5'
 \end{array}$$



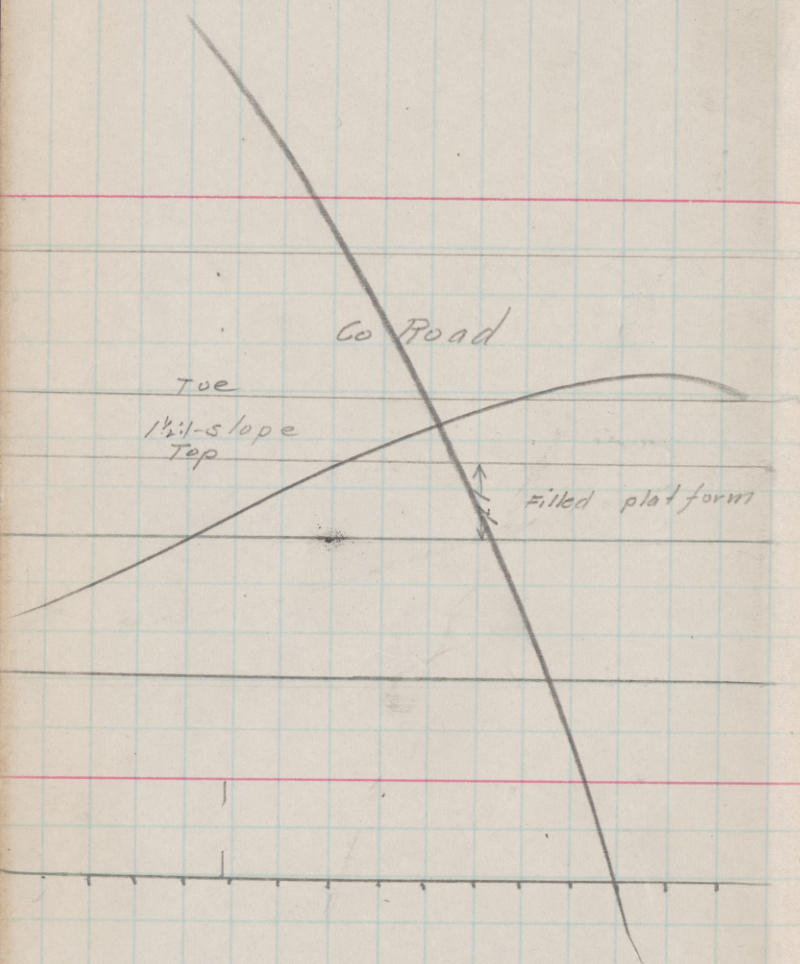
Healdsburg	" 32	Check - Spur for Shell Oil Co. ✓	4-8-15
Healdsburg	" 34	Location - Tracks at Grant Grave/Spur ✓	4-8-15
"	35	" of Water Columns ✓	
Larkspur	36-38	" Creek at 2-36" Concrete Pipes ✓	4-12-15
Monte Rio	42-52	Ties to North Shore Land Co. Subdivision ✓	
Duncan Mills	53	Floor Plan - Depot ✓	
Geyserville	54	Prop. lowering of Culvert ✓	
Santa Rosa	56-61	Location of Creek ✓	
Willits	62-62½	Standard Oil Co. - Prop. Spur ✓	

Index - T-18

①

Fairfax	Page 5-8	Proposed Improvements ✓	1-5-15
Petaluma	" 9	Curbing Around Trees ✓	1-12-15
Ignacio	" 10	Proposed Fence Extension & Ditch Changes ✓	4-21-15
"	" 11	X-Sections for " " " ✓	1-21-15
Sears Pt.	" 12-13	Quarries - Locating Ellwood Fence ✓	1-26-15
Schellville	" 14	Locating 36" Concrete Pipe ✓	
Sebastopol	" 15-16	Enterprise Brew. Co. & Berry Growers Spur ✓	2-16-15
Highlands	" 17	1st Crossing West of ✓	2-20-15
Bellvue	" 18	X-Sections and Drainage ✓	2-24-15
Santa Rosa	" 19	Proposed Engine Storage -	2-24-15
Mill Valley	" 21-4	Proposed Spur for C.E. Christley ✓	3-10-15
Sears Point	" 25	Fence for Mr. Rofforri ✓	3-26-15
Greenwood	" 26	Proposed Drainage (✓	3-26-15
Manor	" 30	X Sections ✓	4-6-15
Manor	" 31	Survey of Ground - Prop. to Buy ✓	4-6-15

60
steps 2 9 19 700

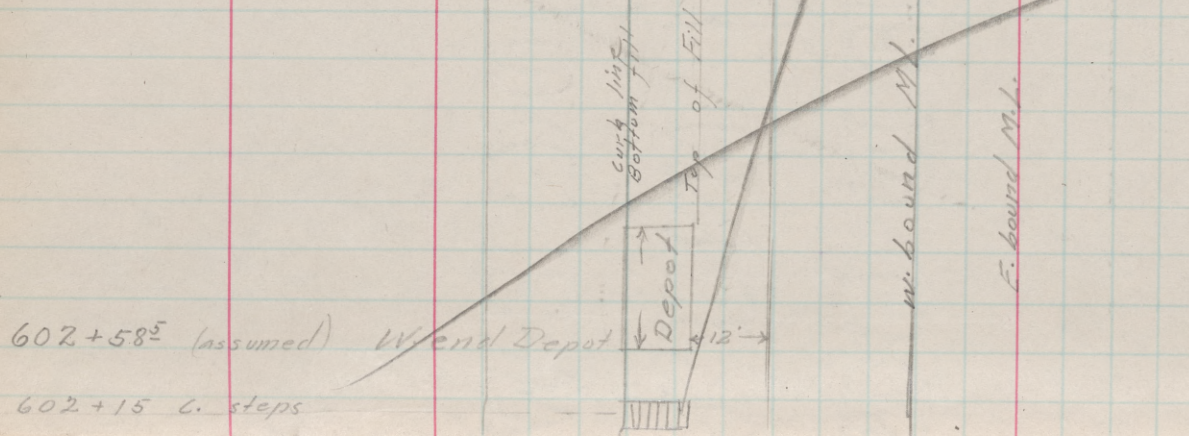


FAIRFAX - PROPOSED IMPROVEMENTS

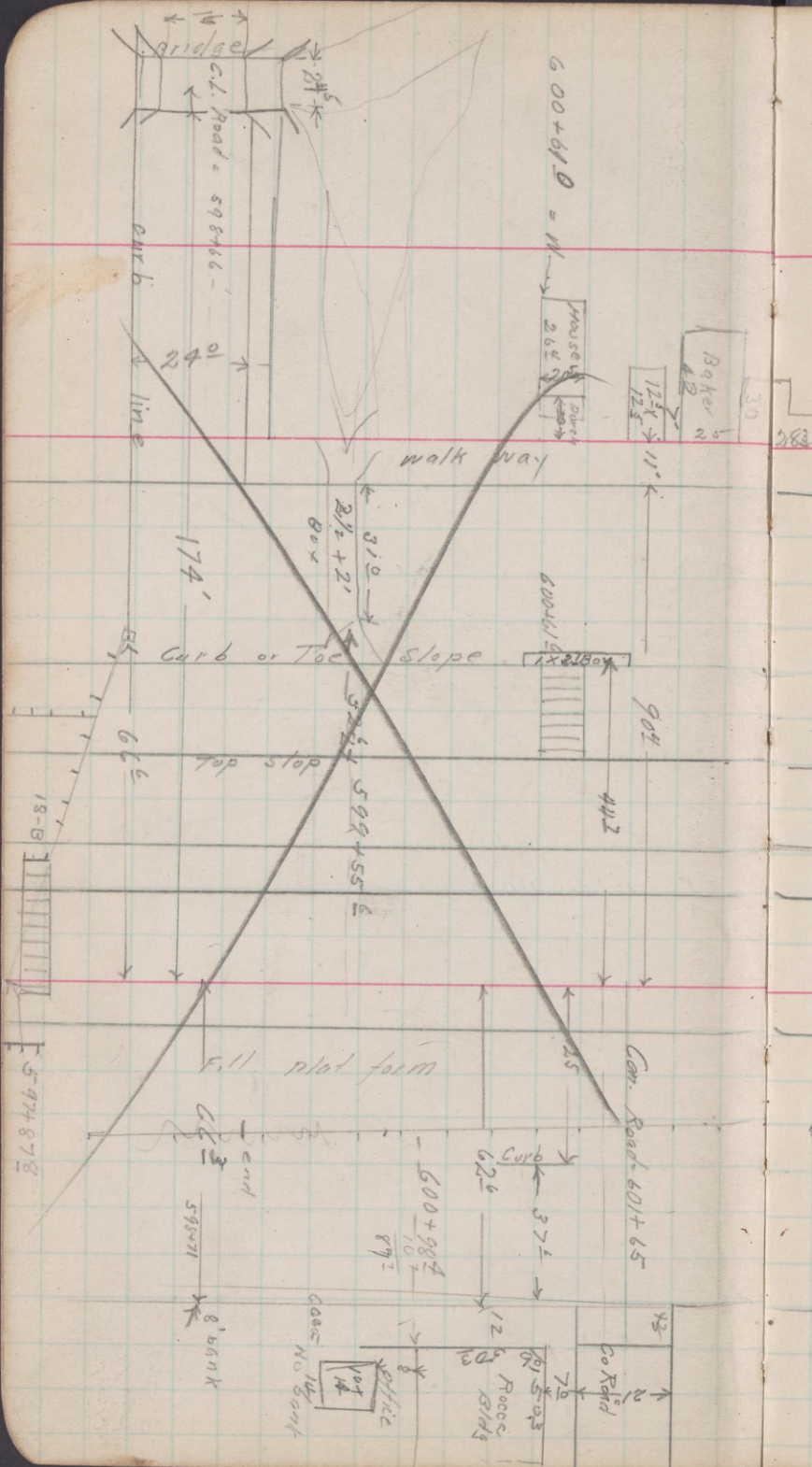
(2)

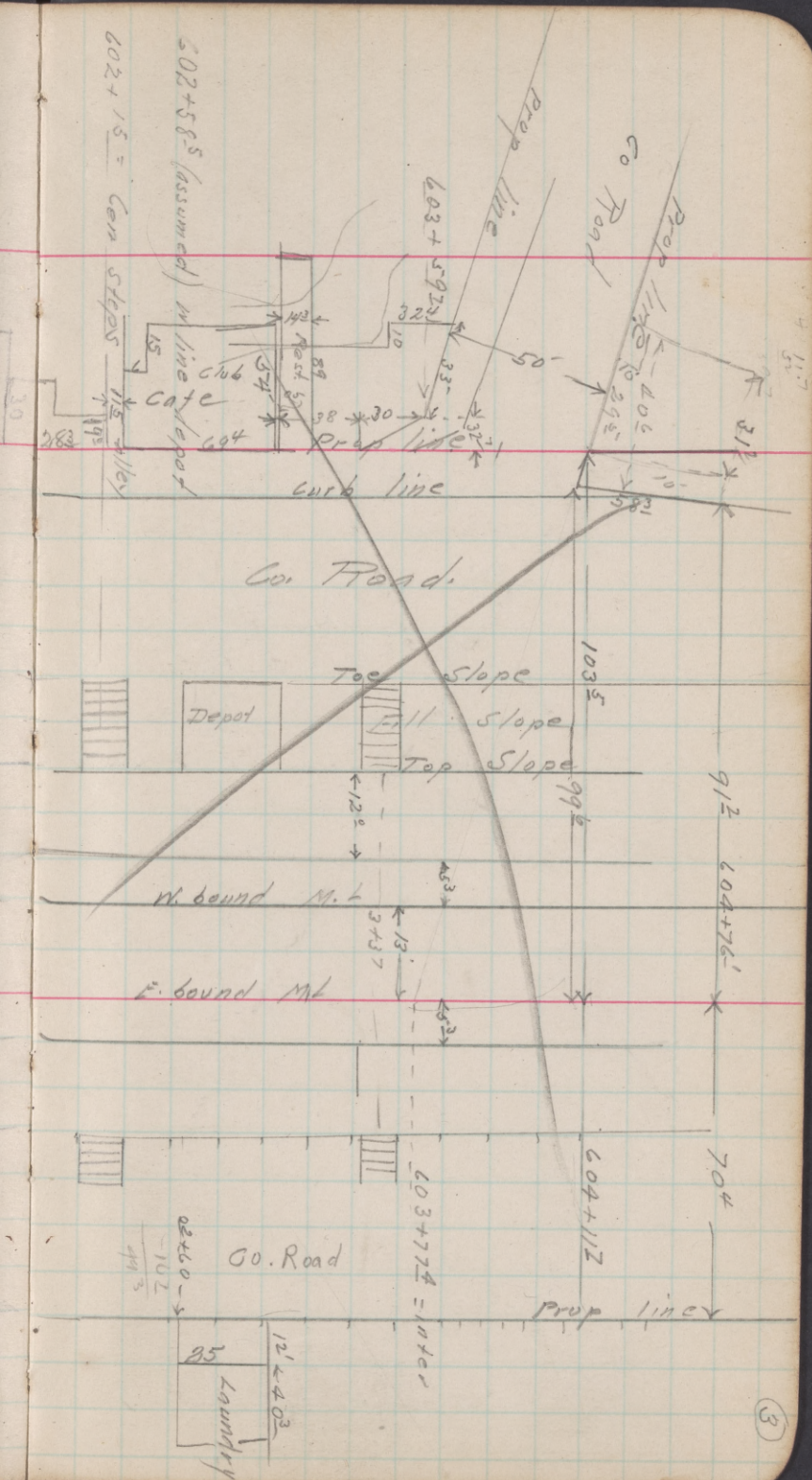
JAN. 6, 15.

J.F.B.
W.J.A.
G.L.B.



6
687+66





Handwritten marks and symbols on the right edge of the page, including a large 'X' and some illegible characters.

0

1

8

7

(4)

+

8

2

1

604+00

$$\frac{-63}{93} \text{ CR } \frac{-64}{71} \frac{-74}{49} \frac{-52}{42} \frac{-09}{29} \frac{+11}{182} \frac{0}{18} \frac{0}{2} \frac{0}{5} \frac{+06}{52} \frac{+04}{11} \frac{-35}{17} \frac{-31}{38} \text{ CR } \frac{-45}{38} \frac{-45}{60} -$$

603+00

$$\frac{\text{curb}}{94} \frac{-62}{94} \text{ CR } \frac{-67}{73} \frac{-66}{63} \frac{-81}{49} \frac{+12}{29} \frac{+11}{182} \frac{0}{18} \frac{0}{2} \frac{0}{5} \frac{+08}{52} \frac{+06}{12} \frac{-07}{14} \frac{10}{17} \frac{-37}{21} \frac{-22}{37} \text{ CR } \frac{-38}{50}$$

602+00

$$\frac{-62}{91} \frac{-58}{71} \frac{-60}{47} \frac{+06}{28} \frac{+09}{182} \frac{-0}{18} \frac{0}{2} \frac{0}{5} \frac{+08}{52} \frac{+03}{14} \frac{-42}{23} \frac{-30}{38} \text{ CR } \frac{-28}{63}$$

601+00

$$\frac{-64}{86} \text{ CR } \frac{-81}{67} \frac{-52}{67} \frac{-74}{45} \frac{-54}{42} \frac{+15}{28} \frac{+07}{182} \frac{0}{18} \frac{0}{2} \frac{0}{5} \frac{+09}{52} \frac{+05}{145} \frac{-43}{25} \frac{-24}{40} \text{ CR } \frac{-11}{49} \frac{-22}{57} \frac{-22}{63} \text{ curb}$$

600+00

$$\frac{-52}{89} \frac{-45}{79} \text{ CR } \frac{-32}{69} \frac{-50}{50} \frac{-78}{46} \frac{-54}{43} \frac{+03}{29} \frac{+08}{182} \frac{-0}{18} \frac{0}{2} \frac{0}{5} \frac{+09}{52} \frac{+09}{15} \frac{-27}{24} \frac{-10}{37} \text{ CR } \frac{-14}{37} \frac{-14}{54} \frac{-14}{74}$$

599+00

$$\frac{-50}{83} \text{ CR } \frac{-22}{63} \frac{-31}{63} \frac{-43}{49} \frac{+03}{40} \frac{+08}{31} \frac{0}{182} \frac{0}{18} \frac{0}{2} \frac{0}{5} \frac{+09}{52} \frac{00}{17} \frac{-07}{18} \frac{+02}{31} \text{ CR } \frac{+10}{31} \frac{+72}{70} \frac{+72}{72}$$

598+55

$$\frac{-30}{63} \frac{-10}{40} \frac{0}{23} \frac{0}{2} \frac{0}{3} \frac{+07}{8} \frac{+09}{25} \text{ CR } \frac{-03}{25} \frac{+14}{39} \frac{+84}{42} \frac{+84}{51} \text{ Top bank}$$

597+90

$$\frac{-30}{65} \frac{0}{50} \frac{+03}{42} \frac{+12}{35} \frac{+13}{145} \frac{-03}{18} \frac{0}{15} \frac{0}{2} \frac{0}{6} \frac{+14}{9} \frac{+28}{24} \text{ CR } \frac{+30}{24} \frac{+53}{37} \frac{+118}{41} \frac{+118}{52} \text{ Top bank}$$

FAIRFAX Proposed Improposed

Levels for relative elevations

J.F.B.

Jan. 7 '15

(5)

Sta. or Location

+S

M.I.

-S

Elev.

B.M. on N.E. Cor (Lt. End) coping of 18-C E1 = 111.667

7.70

119.37

598+6.5 = G. R.R.

7.85

111.52

opp 598+6.5 = G. Wagon Road

11.1

108.27

603+00 = G. R.R.

4.3

115.07

opp 603+00 = G. Wagon Road

10.8

108.57

605+00 = G. R.R.

2.8

116.57

opp 605+00 = G. Wagon Road

5.6

113.77

X. Section's from over G.R.R. 300' each side Depot.

-LT-

606+00

CR 79

-10 79

CR 54

-10 54

+04 32

+07 15

0 C

-07 17

-RT-

-14 20

-21 26

-40 27

-28 28

CR 44

-17 52

-06 62

605+00

-22 88

CR 70

-24 70

+03 28

+06 15

0 C

+01 55

-21 27

-20 41

CR 41

-30 50

-24 60

-24 70

62-

Co. Road.

creek

Co. Bridge

600+610
502

205 Ho.
26th

Co. Road

2 1/2 x 2.80x

+ 552 CL CO ROAD

+31.80x

curb.

45'

52'

101

60

9'

66'

600+97
+86³

+61.6
+502

Rocca Bldg

office

No bank

8' bank

= 18-B

597+878

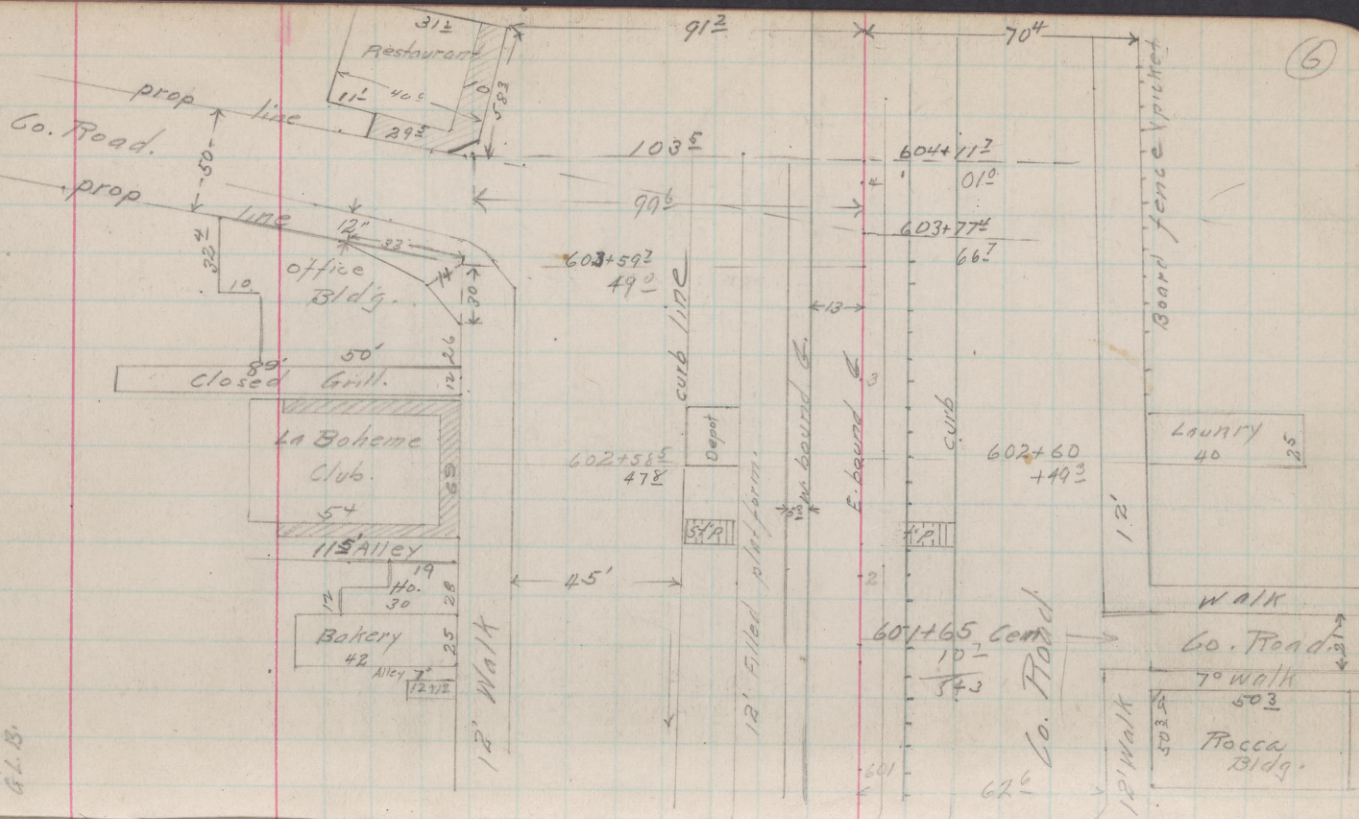
Correction
602+585-602+478
= 102

FAIRFAX.

Proposed Improvements

Jan. 5-1915

J.F.B.
W.A.A.
G.L.B.



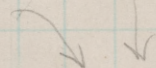
(6)

609+75

$$\frac{\text{Curb}}{49} \quad \frac{+115}{49} \quad \frac{\text{CR}}{37} \quad \frac{+115}{37} \quad \frac{\text{F}}{20} \quad \frac{+102}{19} \quad \frac{+24}{11} \quad \frac{+39}{2} \quad \frac{+14}{40}$$

609+00

$$\frac{\text{Curb}}{49} \quad \frac{+125}{49} \quad \frac{\text{CR}}{36} \quad \frac{+122}{36} \quad \frac{\text{F}}{22} \quad \frac{+116}{20} \quad \frac{+18}{99} \quad \frac{+18}{5} \quad \frac{+35}{2} \quad \frac{0}{4}$$



608+50

$$\frac{\text{Curb}}{53} \quad \frac{+105}{53} \quad \frac{\text{CR}}{40} \quad \frac{+102}{40} \quad \frac{\text{F}}{26} \quad \frac{+112}{24} \quad \frac{+42}{13} \quad \frac{+20}{10} \quad \frac{+12}{5} \quad \frac{+29}{2} = 15' \text{ L/O of M.L. } \frac{0}{36} \text{ R+Spur}$$

608+00

$$\frac{\text{Curb}}{56} \quad \frac{+86}{56} \quad \frac{\text{CR}}{42} \quad \frac{+84}{42} \quad \frac{\text{F}}{26} \quad \frac{+63}{24} \quad \frac{+13}{17} \quad \frac{+03}{5} \quad \frac{0}{2}$$

607+75

$$\frac{\text{Curb}}{56} \quad \frac{+72}{56} \quad \frac{\text{CR}}{43} \quad \frac{+73}{43} \quad \frac{\text{F}}{27} \quad \frac{+53}{27} \quad \frac{+39}{20} \quad \frac{+14}{18} \quad \frac{+06}{5} \quad \frac{0}{2}$$

607+50

$$\frac{\text{Curb}}{55} \quad \frac{+53}{55} \quad \frac{\text{CR}}{44} \quad \frac{+57}{44} \quad \frac{\text{F}}{31} \quad \frac{+50}{31} \quad \frac{+20}{26} \quad \frac{+07}{45} \quad \frac{0}{2}$$

$\frac{00}{2} = \text{spur } \swarrow$

607+00

$$\frac{\text{Curb}}{56} \quad \frac{+22}{56} \quad \frac{\text{CR}}{45} \quad \frac{+23}{45} \quad \frac{+09}{34} \quad \frac{+01}{19} \quad \frac{0}{2}$$

FAIRFAX Proposed Improvements

(7)

Jan. 7-15

J.F.B.
W.G.A.
G.L.B.

Cross Sections 500' East of Depot

For improvement of unloading facilities

F = fence

C.R. = Crown of road.

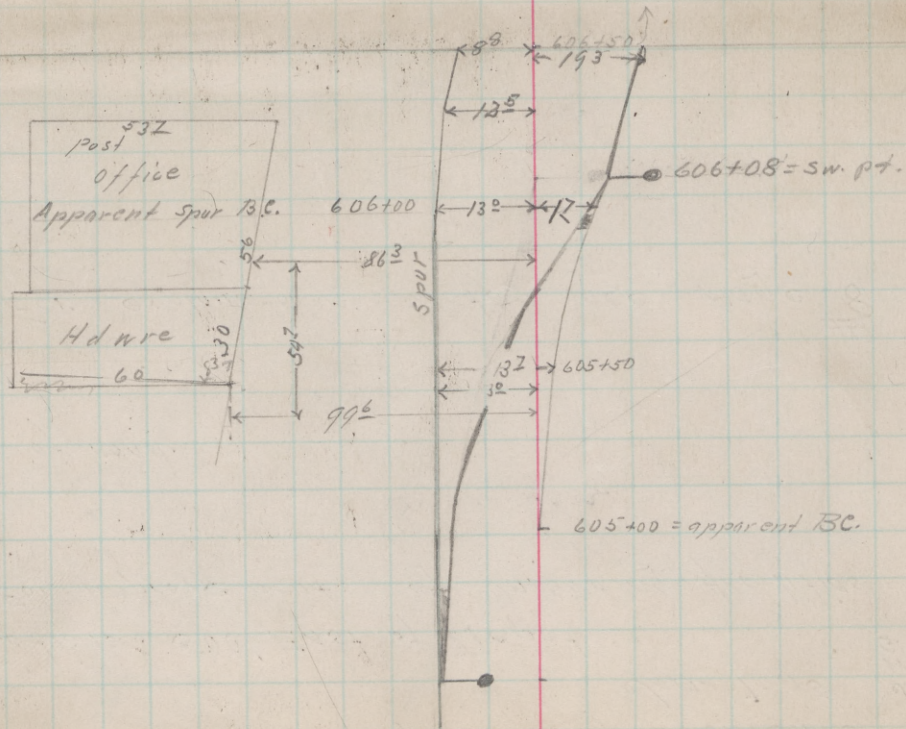
For explanatory sketch see page #8

610+50

00
40

00

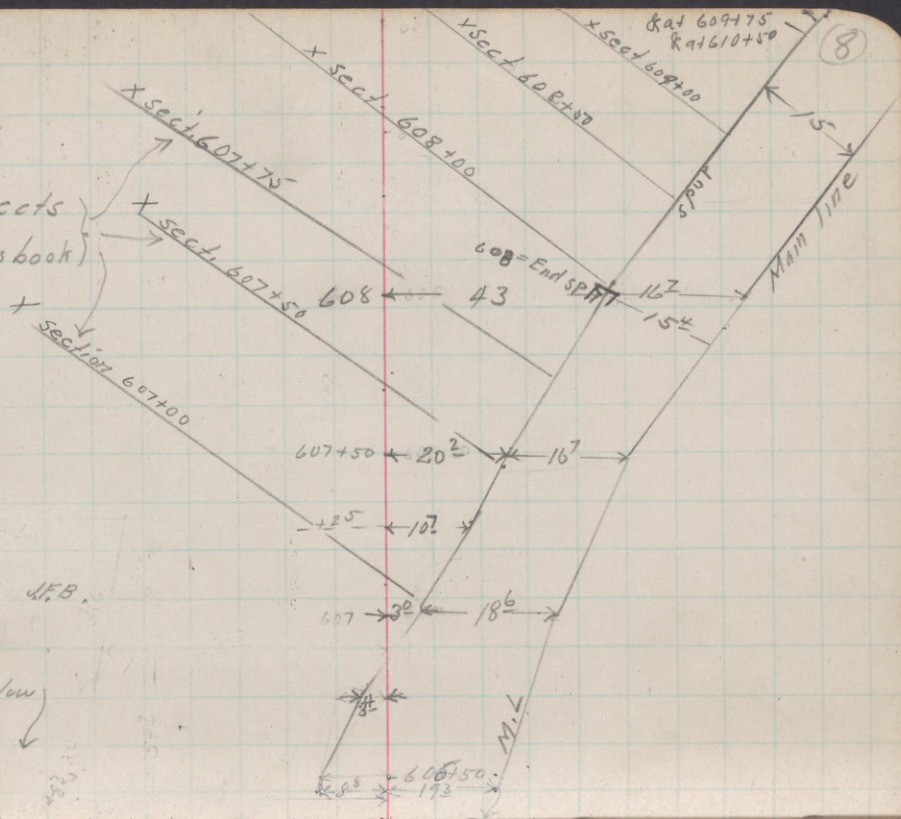
605+50 = W. Line Hdw bldg

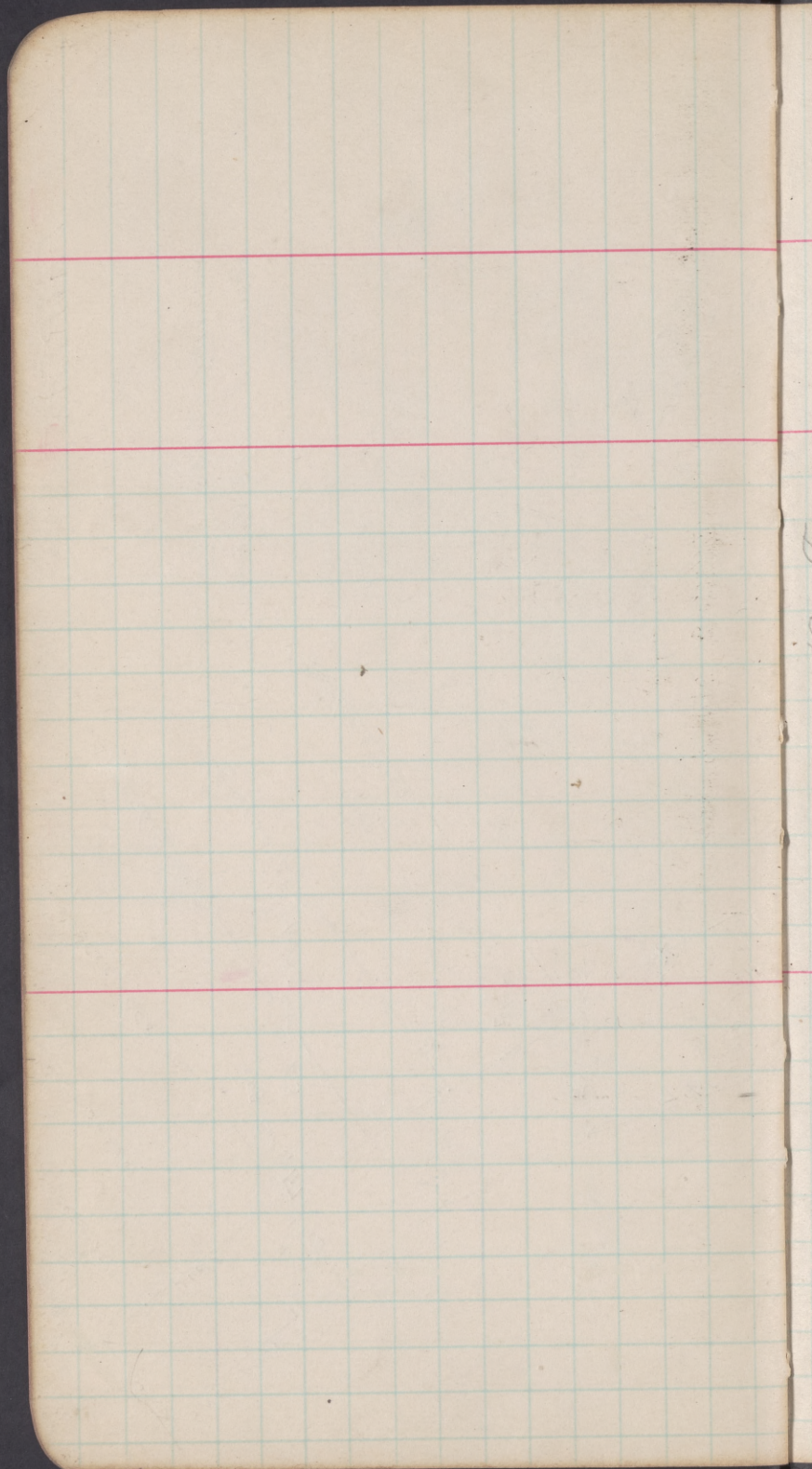


Pt. 5 = 604+53.3

FAIRFAX

showing lines of Xsects
shown on page #7. this book



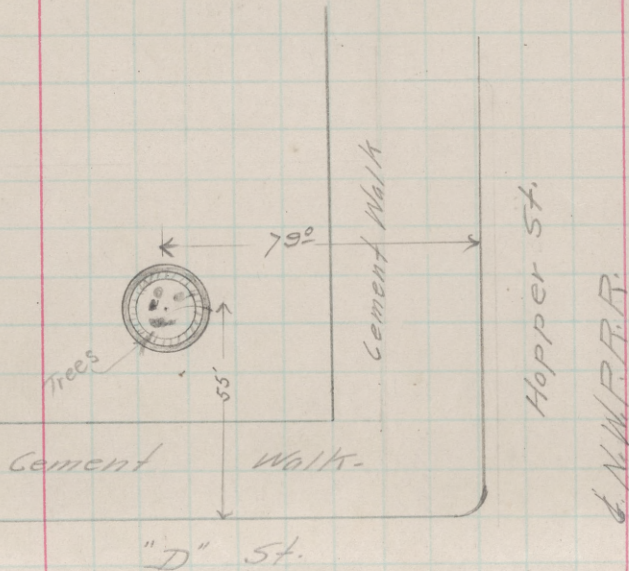


PETALUMA Curbing around Trees

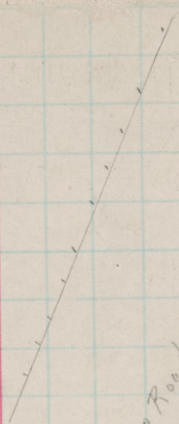
Jan. 12-15

G.F.B.
G.L.B.
J.J.F.

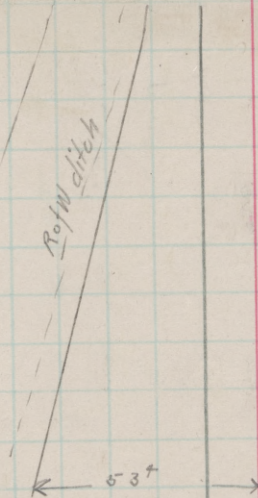
9



1228+00



Go Road



RofW ditch

5.3'

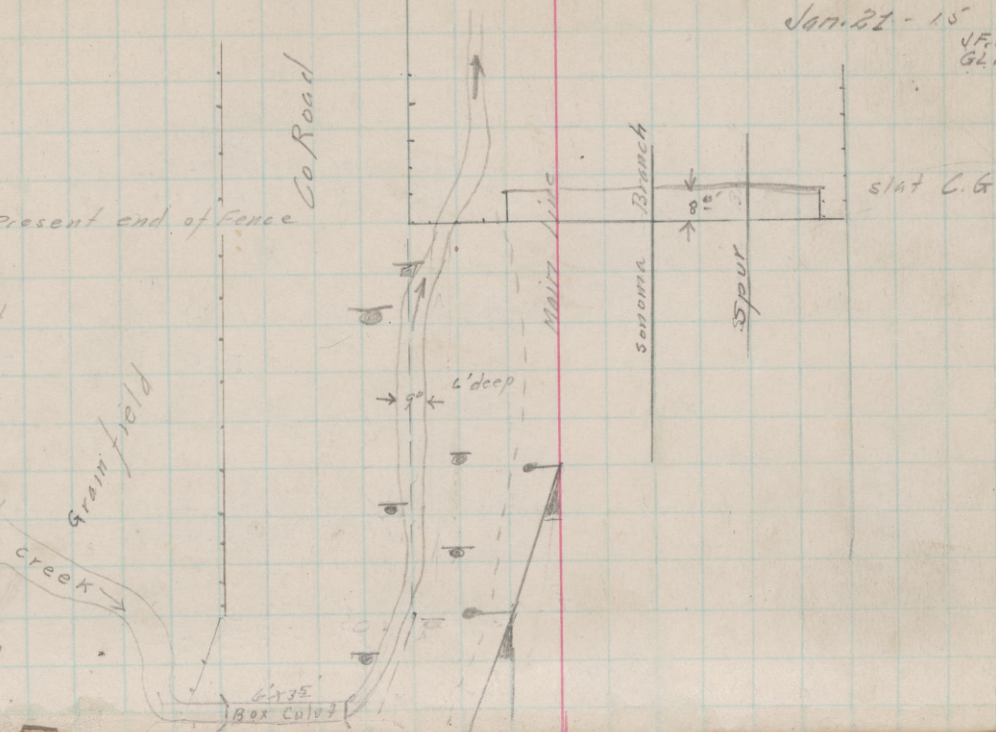
Cross section notes
on Page 11.

IGNACIO - Proposed Fence Extension & Ditch Change. (10)

Jan. 21 - 15

J.F.B.
G.L.B.

- Do not check
OK → 382
1233+25 ← Fence Xing & Present end of Fence
33+35 Tel pole 23' Lt
32+88 Tel pole 26' Lt
32+25 Tel pole 17' Lt
1231+38 Pt. SW
31+54 Tel pole 36' Lt
31+15 Tel pole 20' Lt
1230+77 Pt. SW
30+50 Tel pole 44 1/2' Lt
1229+72 Culvert 50' Lt



32+00

$$\frac{CR}{53} \quad +44 \quad +39 \quad +26 \quad +24 \quad -21 \quad -21 \quad +25 \quad +25 \quad -10 \quad 0 \quad 0$$

$$53 \quad 44 \quad 39 \quad 30 \quad 25 \quad 25 \quad 19 \quad 16 \quad 11 \quad 8 \quad 0$$

32+50

$$\frac{CR}{52} \quad +36 \quad +34 \quad +23 \quad +30 \quad -22 \quad -21 \quad +18 \quad +18 \quad -11 \quad 0 \quad 0$$

$$52 \quad 44 \quad 37.5 \quad 28.5 \quad 23.5 \quad 21 \quad 18 \quad 15 \quad 9.5 \quad 5.5 \quad 0$$

33+00

$$\frac{CR}{52} \quad +34 \quad +20 \quad +25 \quad -10 \quad -21 \quad -21 \quad 0 \quad 0 \quad -13 \quad 0 \quad 0$$

$$52 \quad 34 \quad 24 \quad 20 \quad 19.5 \quad 16 \quad 15.5 \quad 12 \quad 10 \quad 5 \quad 0$$

1233+38

$$\frac{CR}{52} \quad +34 \quad +20 \quad +24 \quad +13 \quad -20 \quad -20 \quad -08 \quad -08 \quad 0 \quad 0$$

$$52 \quad 34.5 \quad 25 \quad 18.5 \quad 15.4 \quad 13 \quad 10 \quad 7 \quad 5 \quad 0 \quad 0$$

1233+50

$$\frac{F}{25} \quad +30 \quad +31 \quad -22 \quad -22 \quad 0 \quad 0$$

$$25 \quad 25 \quad 19 \quad 14 \quad 11.8 \quad 0 \quad 0$$

IGNACIO Cross Sections Proposed Fence Extension 11

Jan. 21-15

V.F.B. - G.L.B.

29+60

$$\begin{array}{r} \text{Edge Rd.} \\ \hline 63 \end{array} \quad \begin{array}{r} +32 \\ \hline 63 \end{array} \quad \begin{array}{r} +41 \\ \hline 35 \end{array} \quad \begin{array}{r} -12 \\ \hline 30 \end{array} \quad \begin{array}{r} -12 \\ \hline 28 \end{array} \quad \begin{array}{r} 0 \\ \hline 27 \end{array}$$

$\frac{0}{2}$

Base of rail = 0.0

29+72

$$\begin{array}{r} \text{Culvert} \\ \hline 63 \end{array} \quad \begin{array}{r} +02 \\ \hline 63 \end{array} \quad \begin{array}{r} -10 \\ \hline 50 \end{array} \quad \begin{array}{r} +31 \\ \hline 44 \end{array} \quad \begin{array}{r} +34 \\ \hline 34 \end{array} \quad \begin{array}{r} -12 \\ \hline 29 \end{array} \quad \begin{array}{r} -12 \\ \hline 27 \end{array} \quad \begin{array}{r} 0 \\ \hline 25 \end{array} \quad \begin{array}{r} 0 \\ \hline 0 \end{array}$$

30+00

$$\begin{array}{r} \text{CR} \\ \hline 70 \end{array} \quad \begin{array}{r} +54 \\ \hline 70 \end{array} \quad \begin{array}{r} +52 \\ \hline 63 \end{array} \quad \begin{array}{r} +34 \\ \hline 56 \end{array} \quad \begin{array}{r} +32 \\ \hline 44 \end{array} \quad \begin{array}{r} -06 \\ \hline 41 \end{array} \quad \begin{array}{r} -06 \\ \hline 39 \end{array} \quad \begin{array}{r} +32 \\ \hline 36 \end{array} \quad \begin{array}{r} +48 \\ \hline 32 \end{array} \quad \begin{array}{r} -14 \\ \hline 27 \end{array} \quad \begin{array}{r} -14 \\ \hline 25 \end{array} \quad \begin{array}{r} 0 \\ \hline 22 \end{array}$$

$\frac{0}{0}$

For

30+50

$$\begin{array}{r} \text{CR} \\ \hline 61 \end{array} \quad \begin{array}{r} 54 \\ \hline 61 \end{array} \quad \begin{array}{r} +50 \\ \hline 55 \end{array} \quad \begin{array}{r} +40 \\ \hline 52 \end{array} \quad \begin{array}{r} +32 \\ \hline 39 \end{array} \quad \begin{array}{r} -06 \\ \hline 36 \end{array} \quad \begin{array}{r} -06 \\ \hline 34 \end{array} \quad \begin{array}{r} +22 \\ \hline 30 \end{array} \quad \begin{array}{r} +42 \\ \hline 27 \end{array} \quad \begin{array}{r} -14 \\ \hline 23 \end{array} \quad \begin{array}{r} 0 \\ \hline 19 \end{array}$$

all main p.

31

$$\begin{array}{r} \text{CR} \\ \hline 57 \end{array} \quad \begin{array}{r} +54 \\ \hline 57 \end{array} \quad \begin{array}{r} +54 \\ \hline 49 \end{array} \quad \begin{array}{r} +38 \\ \hline 40 \end{array} \quad \begin{array}{r} +41 \\ \hline 35 \end{array} \quad \begin{array}{r} -16 \\ \hline 30 \end{array} \quad \begin{array}{r} -16 \\ \hline 26 \end{array} \quad \begin{array}{r} +38 \\ \hline 24 \end{array} \quad \begin{array}{r} +38 \\ \hline 22 \end{array} \quad \begin{array}{r} -12 \\ \hline 15 \end{array} \quad \begin{array}{r} -12 \\ \hline 14 \end{array} \quad \begin{array}{r} 0 \\ \hline 13 \end{array}$$

$\frac{0}{2}$

31+50

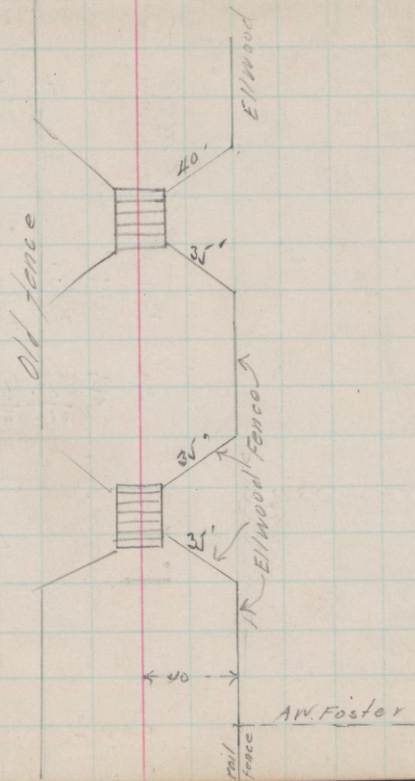
$$\begin{array}{r} \text{CR} \\ \hline 52 \end{array} \quad \begin{array}{r} +52 \\ \hline 52 \end{array} \quad \begin{array}{r} +45 \\ \hline 47 \end{array} \quad \begin{array}{r} +34 \\ \hline 39 \end{array} \quad \begin{array}{r} +41 \\ \hline 30 \end{array} \quad \begin{array}{r} -20 \\ \hline 22 \end{array} \quad \begin{array}{r} -20 \\ \hline 23 \end{array} \quad \begin{array}{r} +38 \\ \hline 19 \end{array} \quad \begin{array}{r} +38 \\ \hline 17 \end{array} \quad \begin{array}{r} -12 \\ \hline 12 \end{array} \quad \begin{array}{r} -12 \\ \hline 10 \end{array} \quad \begin{array}{r} 0 \\ \hline 8 \end{array}$$

$\frac{0}{0}$

94+87
 94+62.5 East end } Trestle 34-A
 94+15.5 West end }
 494+100 Second break in Ellwood fence

73+63 Ellwood Fence recommence
 73+52.5 East end } Trestle 33-F
 73+36.5 West end }
 473+23 First break in Ellwood fence

461+10 Beg. of Ellwood fence on Rt.



SEARS Pt. - QUARRIES - Locating Ellwood fence.

Jan. 26, 1915 (12)

J.F.B. Rain
G.L.B. like

Cont'd next Page

525+64

Ellwood recommence on Rt only - & Rt Gard.

525+40

End Ellwood fence on left & Rt Gard.

523+38

Commence Ellwood fence on left

523+28

22+99⁷

East end

Trestle 34 D

522+67²

West end

522+37

13+46⁰

13+25⁴

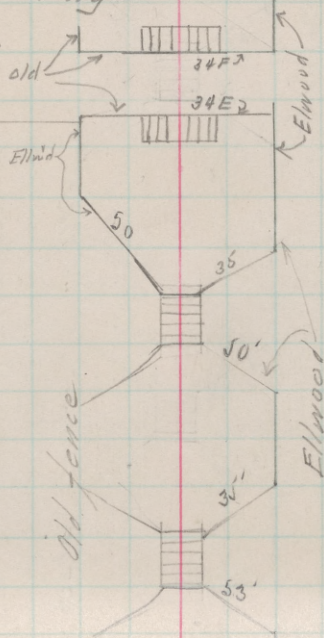
East end

513+09⁴

West end

Trestle 34-B

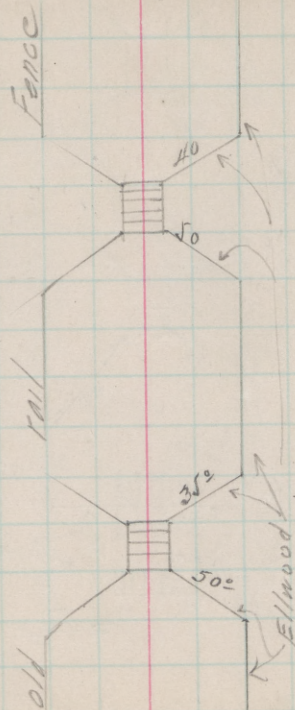
512+61²



600 ft to House →

562+04
 561+64 East end } Trestle 35-B.
 561+32 West end }
 560+82

28+60
 528+22² East end } Trestle 35A
 528+06² West end }
 527+28⁰



SEARS Pt. - QUARRIES - Locating Ellwood fence Jan. 26.

(13)

Jan. 26-'15 J.F.B.
G.L.B.

Note

on Rt. Ellwood fence continuous from $461+10$ to $589+70 = 12,860'$
on Lt. " " " " " " $523+38$ to $525+40 = 202$
total length Ellwood fence $13,062$

$589+70$ End of Ellwood fence on Rt.

821+43

Pl. SW.

Depot

SCHELLVILLE - Locating 36" Concrete Pipe

(14)

on line of S.P. & N.W.P. Transfer tracks.

J.F.B.

G.L.B.

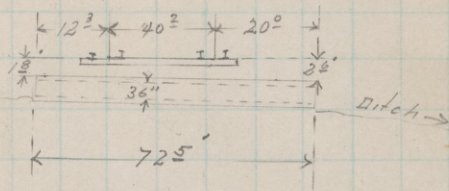
S.P. Line

Napa Inc. →

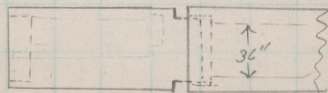
offset fence

X' Sect of Pipe

Field



showing Joints



Pipe appears to
be on S.P. property

S.P.

N.W.P.

36" Con. Pipe
on inner
to pt. SN = 494.0

494.0

3+717
3+58
63

EC

SC. TC = 13°42'

2+233

pt Frog

2+20

BC 8°40'

1617

pt SW

0+592

pt. Frog

6°22' < pt

0+00

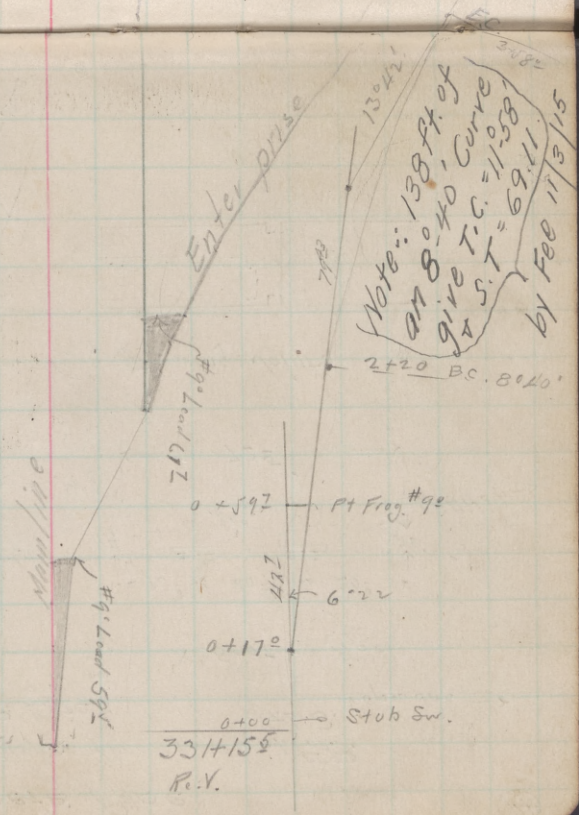
H.B.

stub
pt SW to
main line

House, Enterprise, & Berry Growers

331+159

R.V.



105116

SEBASTOPOL- Enterprise Brew Co. & Berry Growers Spur (15)

9+17⁰

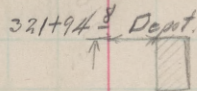
End spur

Feb. 16-15

J.F.B.
W.V.A.

7+27²

EC



T.C. = 10°00'

6+53²

B.C. 13°30' Lt

6+24²

W. end Enterprise platform clear = 6'

Parallel Spur

0+92¹ EC

0+44³ B.C. 7°30' Lt

0+42⁵ = pt Fr

6+05⁴

W. end trestle G to present gage = 22' (plenty room to move ties on stringers)

5+88⁷

E. end trestle G to

5+71⁶

E.C.

0+00
P.I. Fr. A

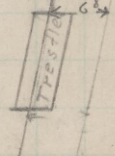
T.C. = 5°15'

4+21³

BC 7°10'

Note.
1350 Mt. to prop.
1304.7 Mt. to spur
Berry Growers foundation
3' 6" back from prop.

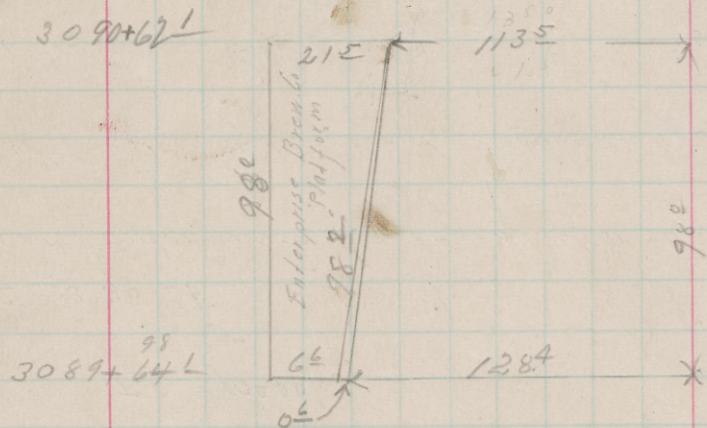
House Track



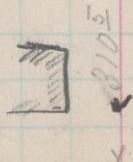
Berry

EC
348'

Sebastopol. Location of Platform Encroachment of
Enterprise Brewing Co. Feb-16-1915



3086+53.6 W.L. Depot. 0 946.1
 W. Line Depot = 3086+53.6



Sta

Sta

+5

HI

-5

Elev

(16)

B.M. = Top of Hydrant cor McKin. St 100. El assumed

6+05

4.00 - 104.00

6.25 97.75 Top Rail

6+05

6' Lt

9.30 94.70 Out let. under trestle

Dia = 16"

6+73

6.08 97.92 Top rail

6+73

SEBASTOPOL.

7.70 96.30 intake M&K Culvert

8+25

Feb. 16 '15

5.50 98.50 Top rail

8+25

6.10 97.90 ground Elev

5.30 98.70 Top rail end spur

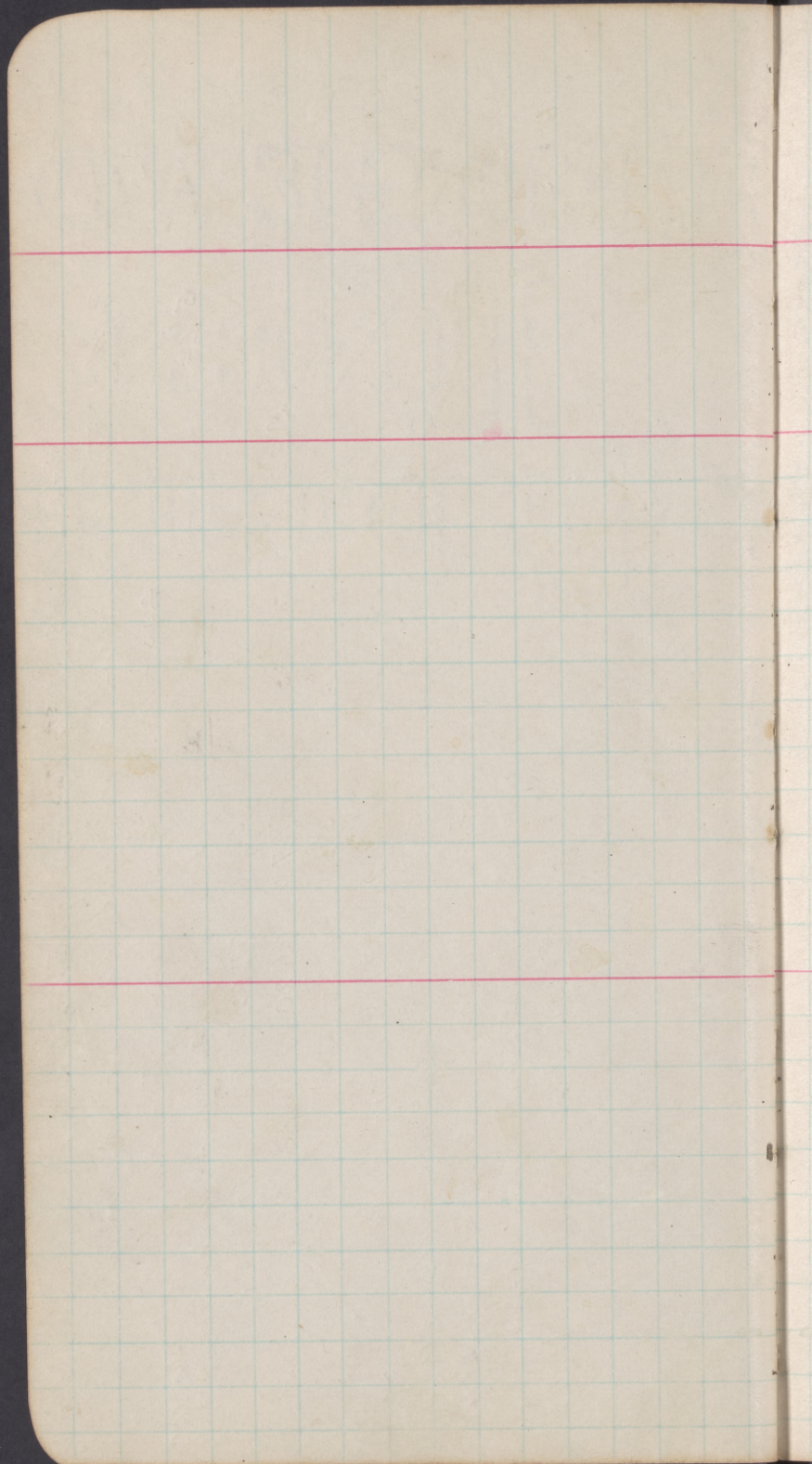
8+25

5.70 98.30 grnd Elev Depot St.

6+75

6.30 97.70 El. under foundation

6.92 97.08 " " "



HIGHLANDS - 1st Crossing West. of.

17

Left

Feb. 20¹⁵ J.F.B.
G.L.B.

dist from W. bound d

E. face 16-E = 0+00 → $\frac{-0^2}{0}$ $\frac{-0^4}{5}$ $\frac{-0^9}{60}$ $\frac{-0^5}{80}$ $\frac{-0^8}{12}$ $\frac{-1^1}{16}$ $\frac{F}{16}$ $\frac{-1^2}{19}$ $\frac{-1^3}{29}$ $\frac{-1^0}{45}$

0+11

0+19

→ $\frac{0}{0}$ $\frac{0}{5}$ $\frac{-0^4}{16}$ $\frac{-0^1}{45}$

0+33

$\frac{0}{0}$ $\frac{0}{4}$ $\frac{-0^5}{13}$ $\frac{-0^6}{18}$ $\frac{-0^6}{29}$ $\frac{-0^6}{40}$

0+40

$\frac{-0^4}{0}$ $\frac{-0^4}{5}$ $\frac{-0^8}{70}$ $\frac{-0^9}{29}$ $\frac{-1^0}{40}$

any water standing opp 0+40
could be very easily ditched
to opening, 15' east of C. & 16' F
ditch would be 28' long, & 15' deep
at deepest part.

cen 16-E = 536 + 10⁶

cen 16-F = 536 + 70⁵

2619+50

$$\begin{array}{cccccccc} -20 & -24 & F & -10 & -10 & -10 & -13 & 0 & 0 \\ 50 & 40 & 29 & 29 & 18 & 11 & 8 & 3 & C \end{array}$$

19+00

$$\text{Level} \begin{array}{cccccccccccc} -20 & -20 & -28 & -20 & -11 & -14 & 0 & 0 & 0 & -13 & -25 & -20 & F \\ 40 & 29 & 22 & 16 & 11 & 8 & 5 & C & 5 & 8 & 19 & 29 & 29 \end{array}$$

18+50

$$\text{Level} \begin{array}{cccccccc} -19 & -20 & -23 & -12 & -11 & 0 & 0 \\ 40 & 29 & 16 & 11 & 8 & 5 & C \end{array}$$

18+00

$$\text{Level} \begin{array}{cccccccc} -20 & F & -20 & -24 & -10 & -16 & 0 & 0 \\ 40 & 29 & 29 & 14 & 10 & 8 & 5 & C \end{array}$$

+50

$$\text{Level} \begin{array}{cccccccc} -16 & -06 & -15 & -10 & -13 & -11 & -13 & 0 & 0 \\ 40 & 29 & 25 & 22 & 17 & 11 & 8 & 5 & C \end{array}$$

17+00

$$\text{Level} \begin{array}{cccccccc} -10 & -11 & -11 & 0 & 0 & 0 & -11 & -11 \\ 29 & 12 & 8 & 5 & C & 5 & 8 & 11 \end{array}$$

2616+50

$$\text{Level} \begin{array}{cccccccccccc} -20 & F & -10 & 08 & -12 & 0 & 0 & 1 & -13 & -10 & -20 & \text{Level} \\ 40 & 29 & 29 & 14 & 8 & C & C & 52 & 10 & 10 & 10 & 10 \end{array}$$

BELLEVUE - Cross Sections & Drainage (18)

Feb 24. J.F.B.
W.S.A.

Assum. EL ground at 51-A bottom of Culvert Low. end = 10.0

" " 26.12 Right side = 9.3

" from 2612 to 2609 = - 0.4%

Willows opp 52-A

51-C 51-D 52-A

Wm. Michie

21+80

21+70

2621+50

2621

2620+00

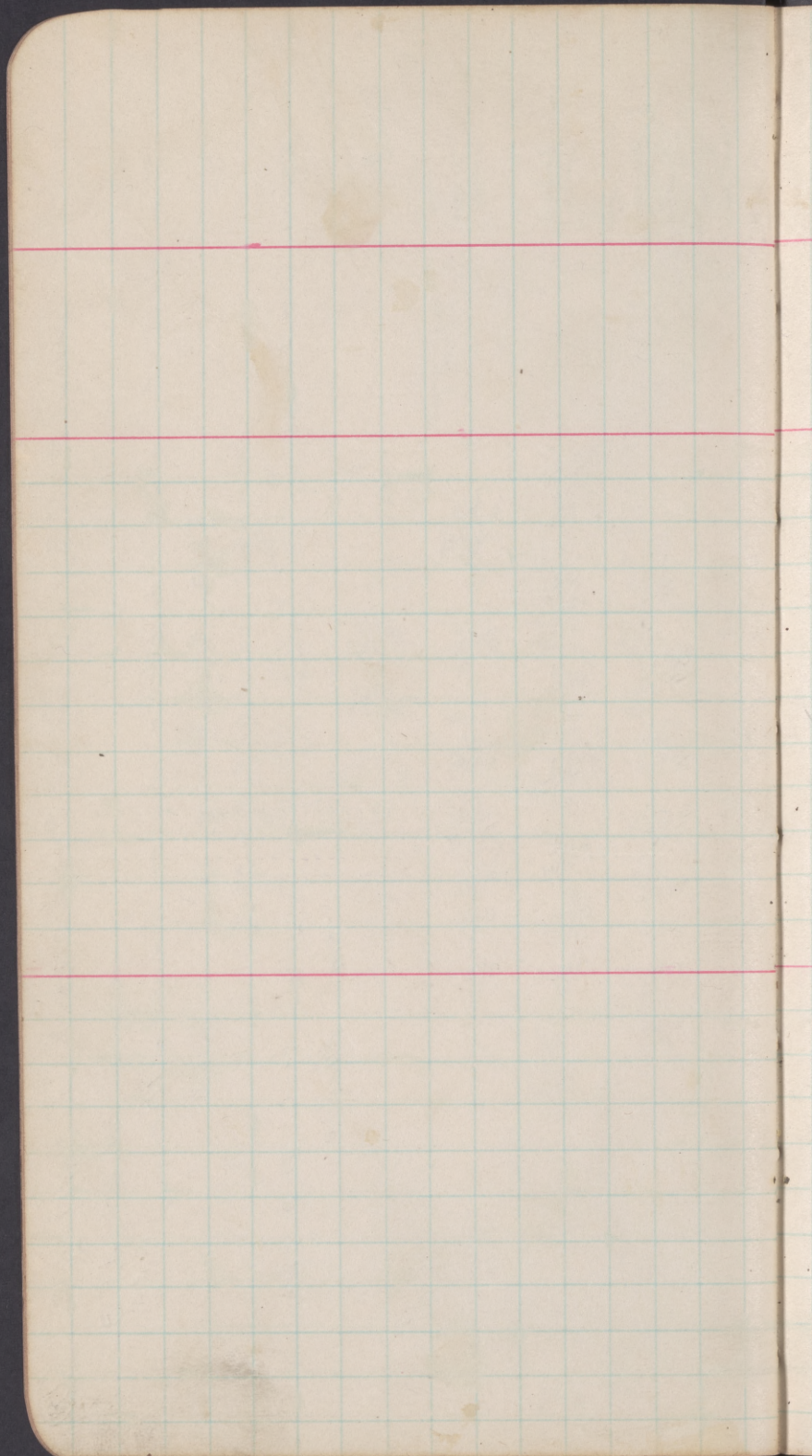
Level

$$\frac{-15}{40} \quad \frac{-15}{30} \quad \frac{-26}{20} \quad \frac{-12}{11} \quad \frac{-13}{8} \quad \frac{0}{5} \quad \frac{0}{C}$$

$$\frac{F}{293} \quad \frac{-22}{29} \quad \frac{-31}{21} \quad \frac{-11}{11} \quad \frac{-13}{8} \quad \frac{0}{5} \quad \frac{0}{C}$$

$$\text{Level} \quad \frac{-23}{29} \quad \frac{-26}{19} \quad \frac{-13}{11} \quad \frac{-13}{8} \quad \frac{0}{5} \quad \frac{0}{C}$$

$$\text{Level} \quad \frac{-16}{29} \quad \frac{-23}{29} \quad \frac{-13}{16} \quad \frac{-13}{12} \quad \frac{-13}{8} \quad \frac{0}{5} \quad \frac{0}{C}$$



SANTA ROSA - Proposed Engine Storage

(19)

B.M. 30.00 El. assumed

Feb. 24-15.

+S 238

when in B.M.
J.H.

J.F.B.
W.V.A.

H.1 32.38

-S 8.23 on pipe at 11+60[±] - 14[±] Lt

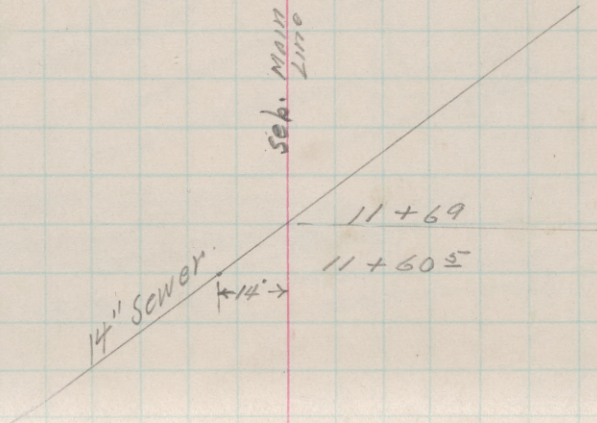
Top of pipe 24.15 " 14" sewer opp. 11+60[±]
intersect at 11+69

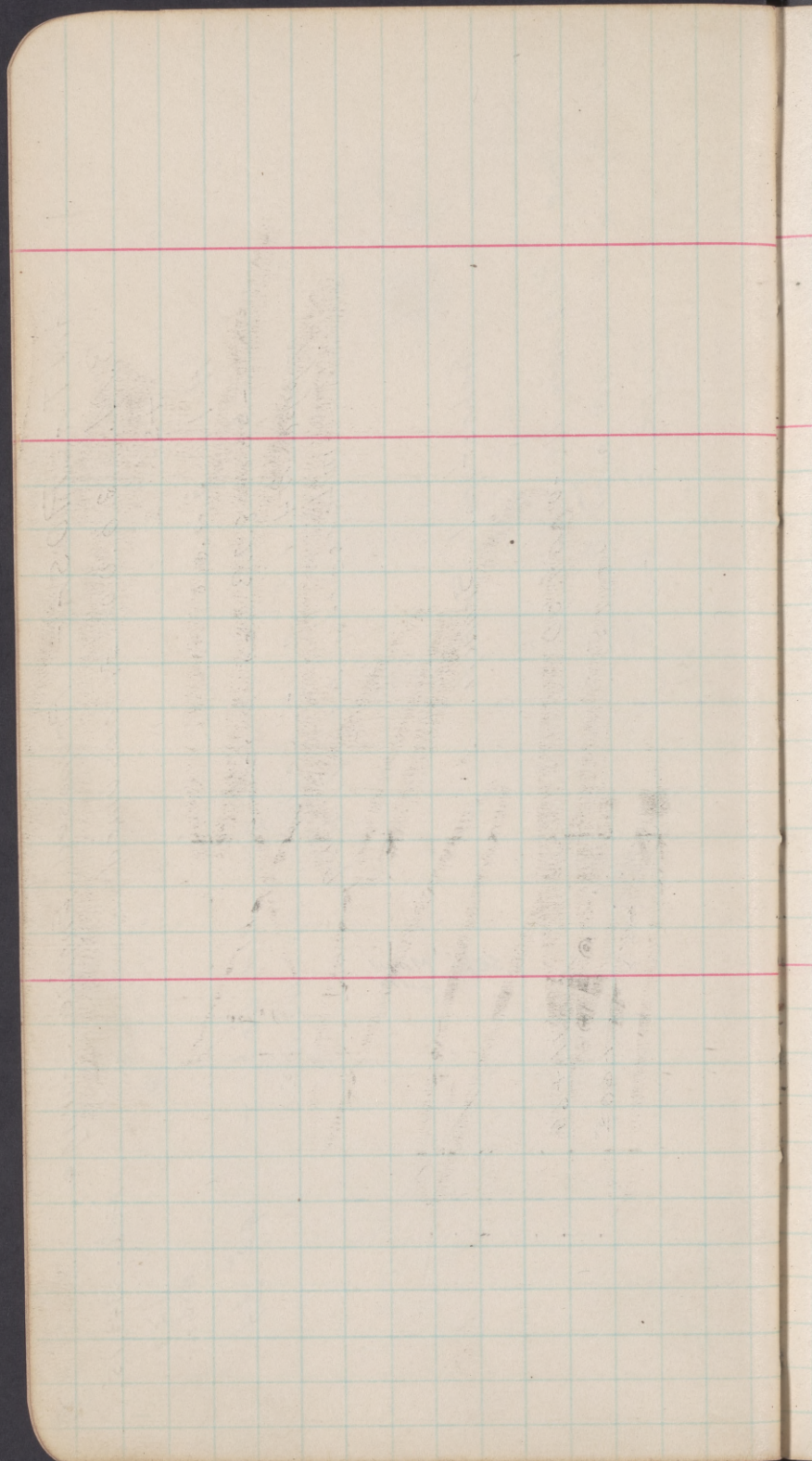
Sebastopol Branch.

El. Base Rail Sta 11+60 = 29.30

El. Top of 14" sewer opp = 24.15

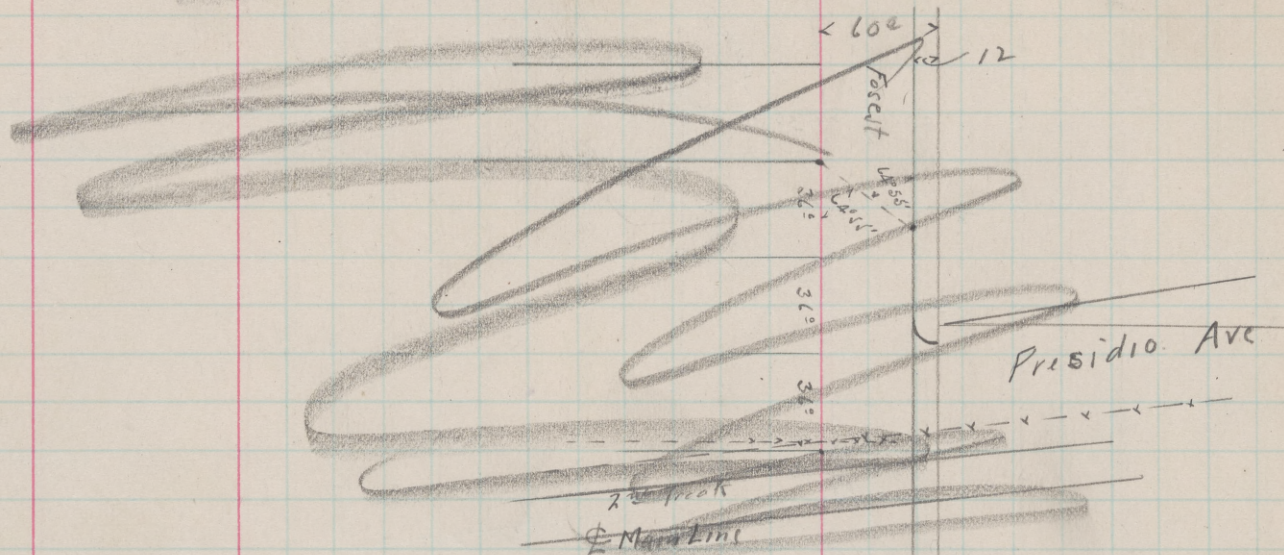
Diff. = 4.15





Mill Valley. Proposed Spur. for.

Mar. 16-15 (20)



81+68⁰ Inter. of St.

81+68⁴ = ⑦ End pwr rail

81+64³ = ⑥ End. pwr rail

+50 = Fence measured

81+04⁶ Pl. frog

80+52⁷ = ④ & 5 = Ends pwr rail

80+35⁰ Pl. SW

80+33 — = ③ = End power Rail

80+18²³ E.C. Pick up. Δ

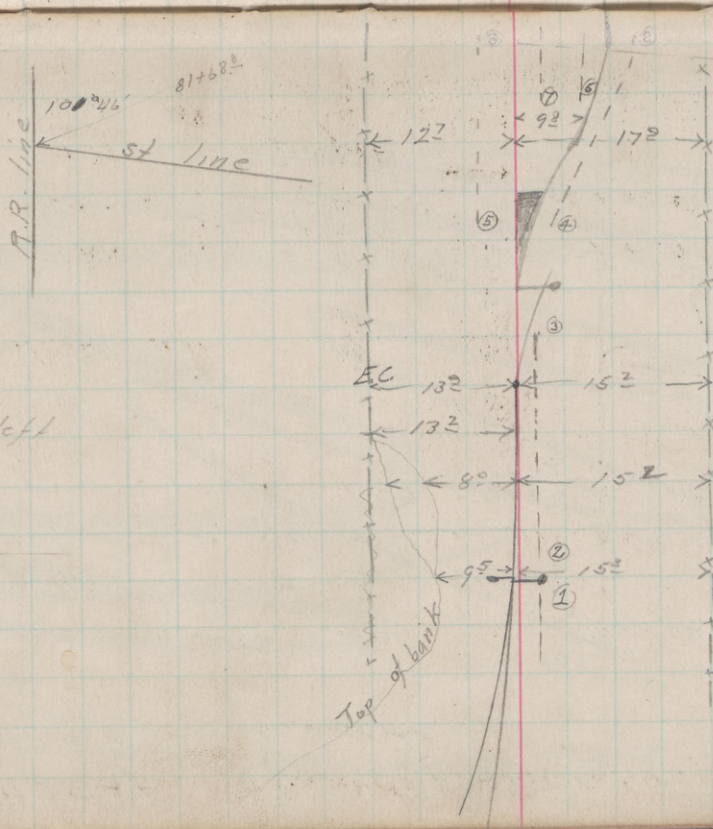
79+61⁵ End fence on left

79+50

79+17⁶ — = ② = End power rail

79+16⁷ Pl SW

79+02⁰ = ① = End pwr rail



Mill Valley. Proposed Spur for G.E. Christley. Mar. 10-15 (21)

83+63⁷

Bulk Head

+50

83+00

82+59⁰

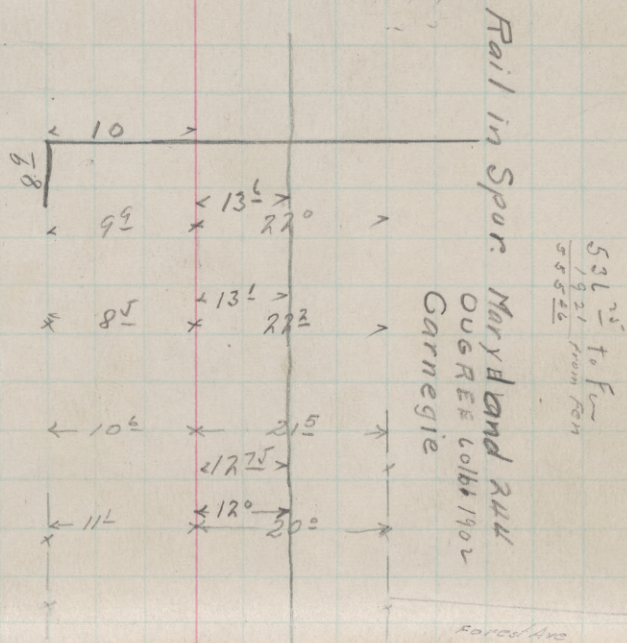
82+50

82+00 Fence measured

81+79² = ⑤ = End pwr. rail

81+77³ = ③ = End pwr. rail

81+68⁶ Inter. of Sp.



2+00
1+87⁶ Pole 2° Rt.

1+18¹⁵ B.C. 16° R 0+00

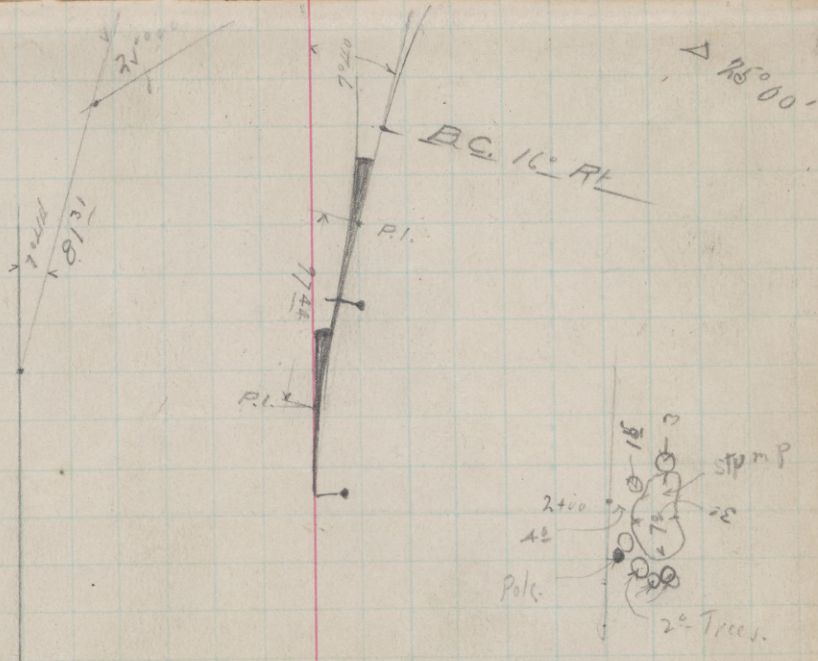
1+66² Pt. Frog 7° 40'

1+00

0+78³ Pole 9° Rt.

0+68⁹ Pt. Frog 7° 40'

0+00
80+35⁹ Pt. S.W. = 0+00



Mill Valley. Proposed Spur for. CE Christley. Mar-10-15 (22)

3 + 24 ⁴⁰ E.C.

12° 30'

3

10° 33'

+ 75

8° 33'

2 + 50 on 4° H. Stamp

6° 33'

Δ 25000

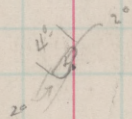
St. 79 ⁴⁵

+ 25

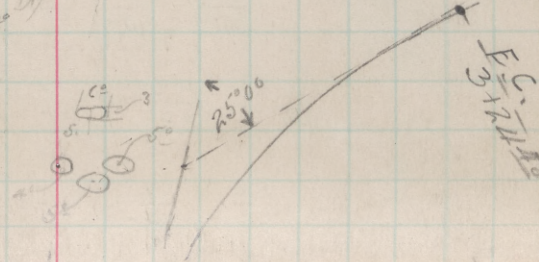
4° 33'

2 + 00

2° 33'



Mr. Christley. will
remove all stamps



3+24.4 E.C.

496 99³

$\frac{-11.5}{18} \leftarrow \frac{Bot Cr.}{18}$

Creek $\frac{-4.3}{17} \rightarrow$ B&K.

$\frac{-2.2}{10}$

$\frac{0.0}{0.0}$

$\frac{-1.5}{13}$

$\frac{-1.6}{34}$

3+00

523 99¹

$\frac{0.0}{38}$

$\frac{-2.3}{31}$

$\frac{-1.7}{26}$

$\frac{0.0}{18}$

$\frac{0.0}{0.0}$

$\frac{-0.2}{20}$

2+75

535 98⁹

$\frac{+0.4}{20}$

$\frac{0.0}{14}$

$\frac{+0.3}{12}$

$\frac{0.0}{0.0}$

$\frac{-0.6}{14}$

$\frac{-1.4}{35}$

2+00

5.1 99²

$\frac{-0.6}{17}$

$\frac{-0.2}{72}$

$\frac{0.0}{0.0}$

$\frac{0.0}{70}$

$\frac{-1.2}{28}$

$\frac{-1.5}{43}$

2+25

64 97⁹

$\frac{+1.0}{17}$

$\frac{+0.4}{11}$

$\frac{+0.5}{8}$

$\frac{0.0}{0.0}$

$\frac{0.0}{35}$

2+00

5.8 98⁵

$\frac{+0.3}{11}$

$\frac{+0.3}{7}$

$\frac{-0.3}{5}$

$\frac{0.0}{0.0}$

$\frac{0.0}{13}$

$\frac{-0.5}{40}$

1+50

~~5.4~~

1+68 ±

6.6 97¹

on Ground.

$\frac{+0.5}{62}$

$\frac{0.0}{0.0}$

$\frac{-0.5}{22}$

$\frac{-0.5}{70}$

1+00

6.6 97¹

$\frac{0.0}{0.0}$

$\frac{-0.6}{70}$

$\frac{-1.4}{8}$

$\frac{-3.5}{13}$

$\frac{-3.0}{32}$

0+68

7.0 97³

0+00

7.13 96⁶

on B.P.

$\frac{0.0}{0.0}$

$\frac{0.0}{4}$

$\frac{-1.8}{12}$

$\frac{-3.4}{17}$

$\frac{-2.6}{34}$

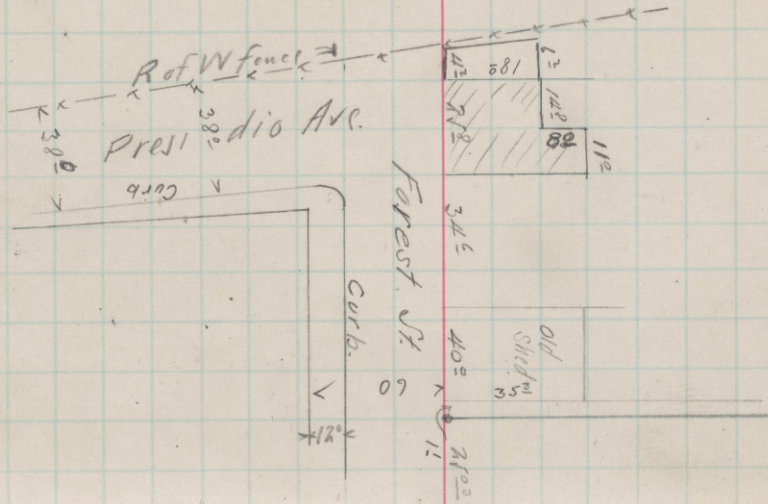
4.33 104.33

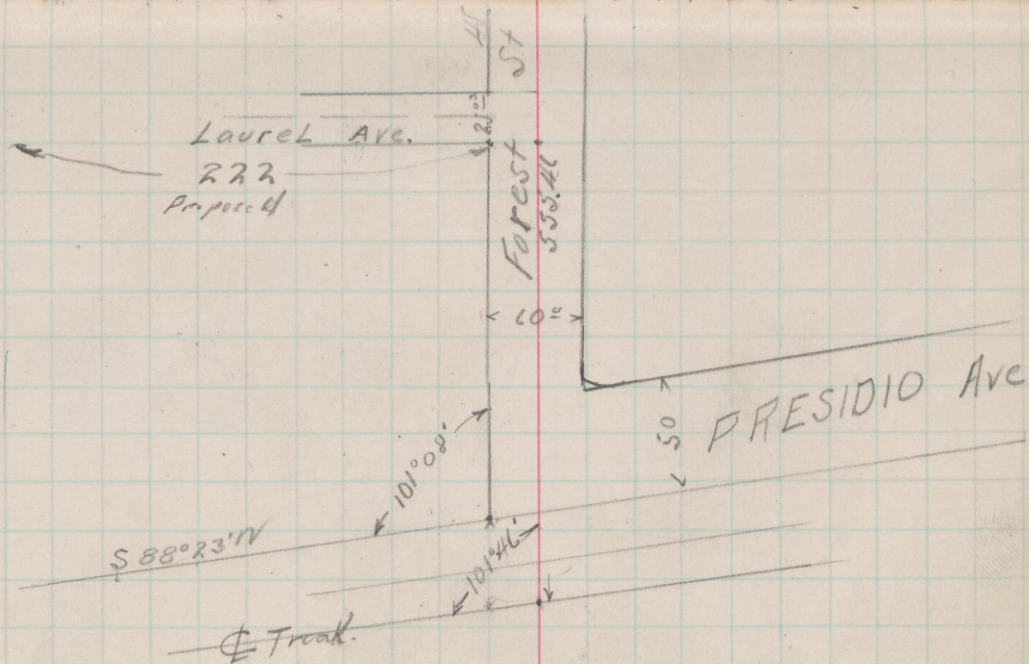
Top of Concrete Abutment. 100⁰⁰ Assump. 11-5

Abutment cys. to
Available for fill

Mill Valley Proposed Spar for GE Christley Mar 10-15 (23)

F.H.G.
J.F.B.
E.B.

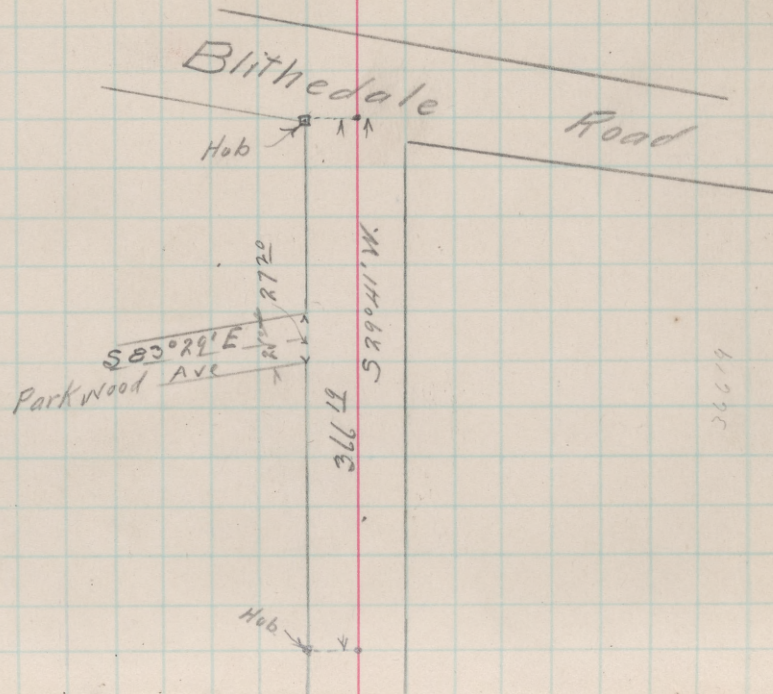


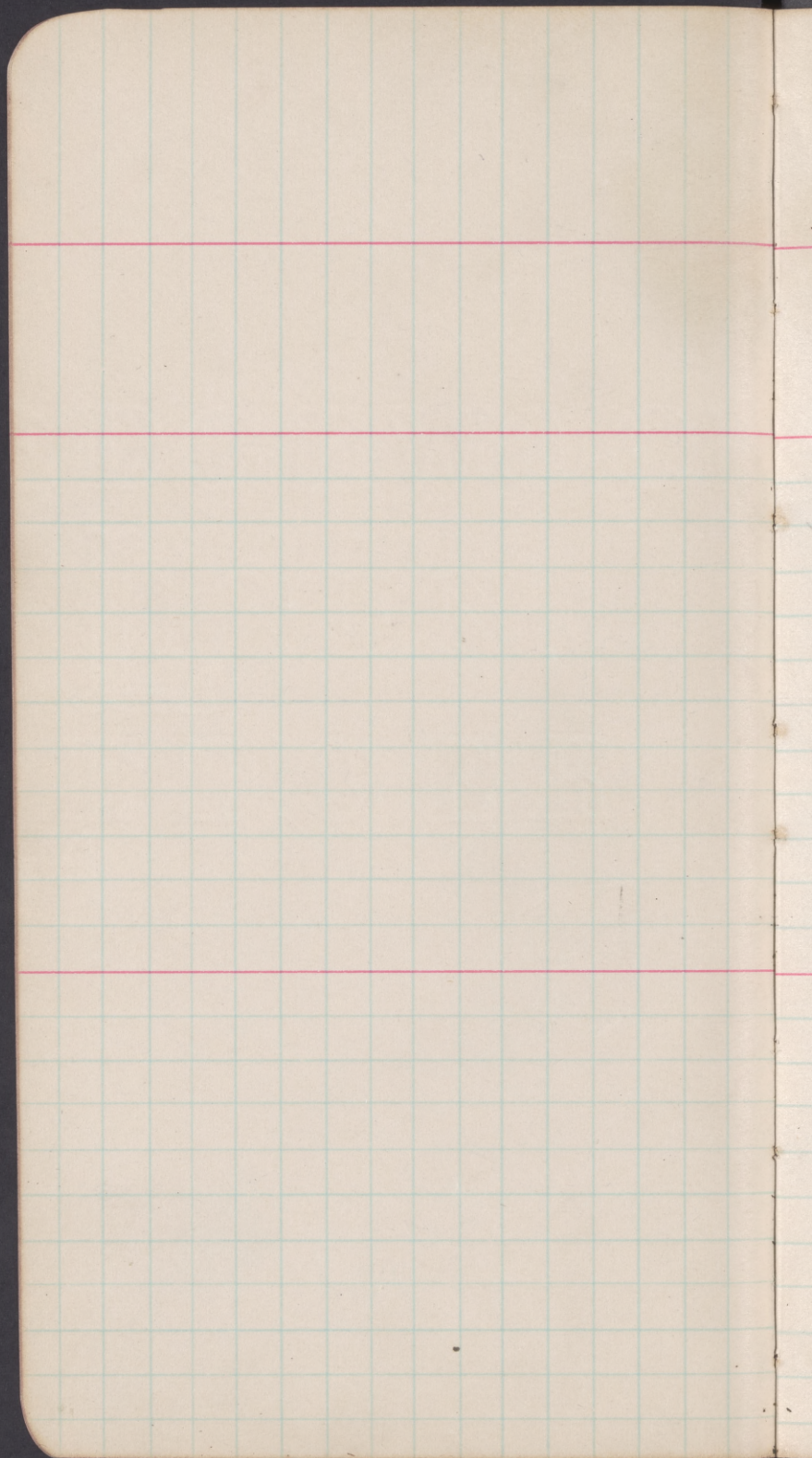


Mill Valley. Proposed Spur for C.E. Christley

Mar. 10-15-

(24)





SEARS POINT - ROFFONI'S FENCE

(25)

1-Mile west of Sears Pt.

9+80 = opp 32-A (3'x2' Culvert)

12+40 to 12+00 = Posts OK rails poor - should have wire

11+50 to 7+50 Post very low & leaning very old B. wire on top

7+50 to 6+50 Fence will be OK for 3yrs if wire is put on top

6+50 to 6+00 should be rebuilt is very poor

6+00 to 3+60 needs top B. wire

3+60 to 1+50 " top & bottom wire rails are very old

1+50 to 0+00 - " rebuilding

entire fence is in very poor condition

0+00 = 980ft E. of 32 A.

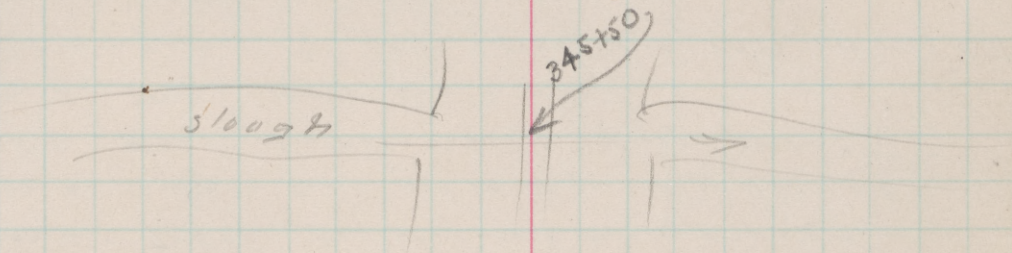
All fences in vicinity are in dilapidated condition

Bed. 31-32 = 181 Rails } 30' Rails
 " 31-30 = 220 "
 11.12. 32 = 300' W. of 31-D

200' West of 31-B

-92° = 918° Slough on Rt & on Lt but no connection -935 = 9065

$\frac{-46}{30}$ $\frac{-32}{29}$ $\frac{-31}{16}$ $\frac{-12}{10}$ $\frac{-02}{4}$ $\frac{0}{6}$ $\frac{-05}{11}$ $\frac{-13}{9}$ $\frac{-30}{14}$ $\frac{-32}{15}$ $\frac{-44}{21}$ $\frac{-42}{29}$



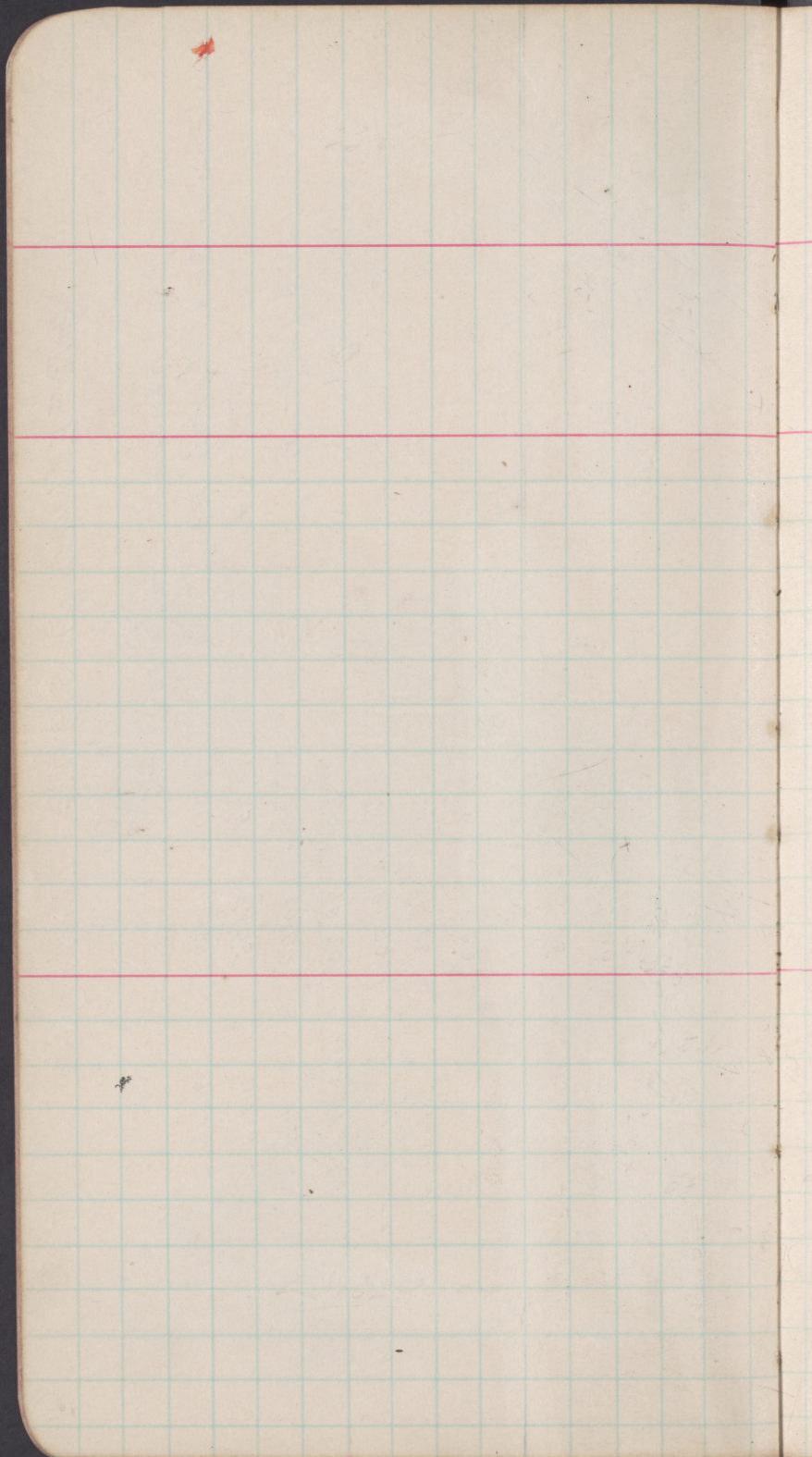
GREENWOOD SPUR - Drainage

(26)

Sta.

Assumed H.I. = 100 - 5

100' East of 31-A (Trestle) Rt.	920	90 80	Ditto
" " " " Lt	925	90 75	Ditto
50' West 31-B (Cattle Guard) Rt	940	90 60	Ditto
50' " " " " Lt	920	90 80	bank of ditch - top of standing W.
350' East 31-B (" ") Lt	830	91 70	top of tie front Wh house
350 " 31-B (" ") Rt	1060	89 40	bottom ditch W = 12 deep
150 " " " (" ") Lt	980	90 20	
150 " " " (" ") Rt	1060	89 40	bottom ditch
100' East of 31-A	455	95.45	Top of tie M.L.
100' " " 31-A - 150' Lt	80	92.00	in field
250 East 31-B - 150 Lt	840	91 60	" "
300 " 31-B -	530	94 70	Top of tie M.L.



10

130

C

28

29

-MAJOR-

-LEVELS-

TO SHOW LAY OF LAND BY
X-SECTION.

STA. 628+25.2

top of 00.

<u>-0.5</u>	<u>-2.6</u>	<u>-3.4</u>	<u>-9.0</u>	drop. 11 to H ₂ O.
25.5	35.5	46.5	137.5	

STA. 627+00-

<u>00</u>	<u>-3.7</u>	<u>-5.0</u>	<u>-5.5</u>	<u>-8.5</u>	<u>-8.5</u>	<u>-8.7</u>	<u>-10.0</u>
240	34	47	67	109	120	132	170

626+00.

<u>-0.5</u>	<u>-4.0</u>	<u>-5.0</u>	<u>-5.2</u>	<u>-7.1</u>	<u>-8.4</u>	<u>-10.0</u>
22	340	46.0	56	75	100	150.0

APRIL-6-1915.

-MATHR-

SURVEY OF PIECE OF
GROUND PROPOSED. TO BUY.

APRIL - 6 - 1915.

M.H. WILSON. T

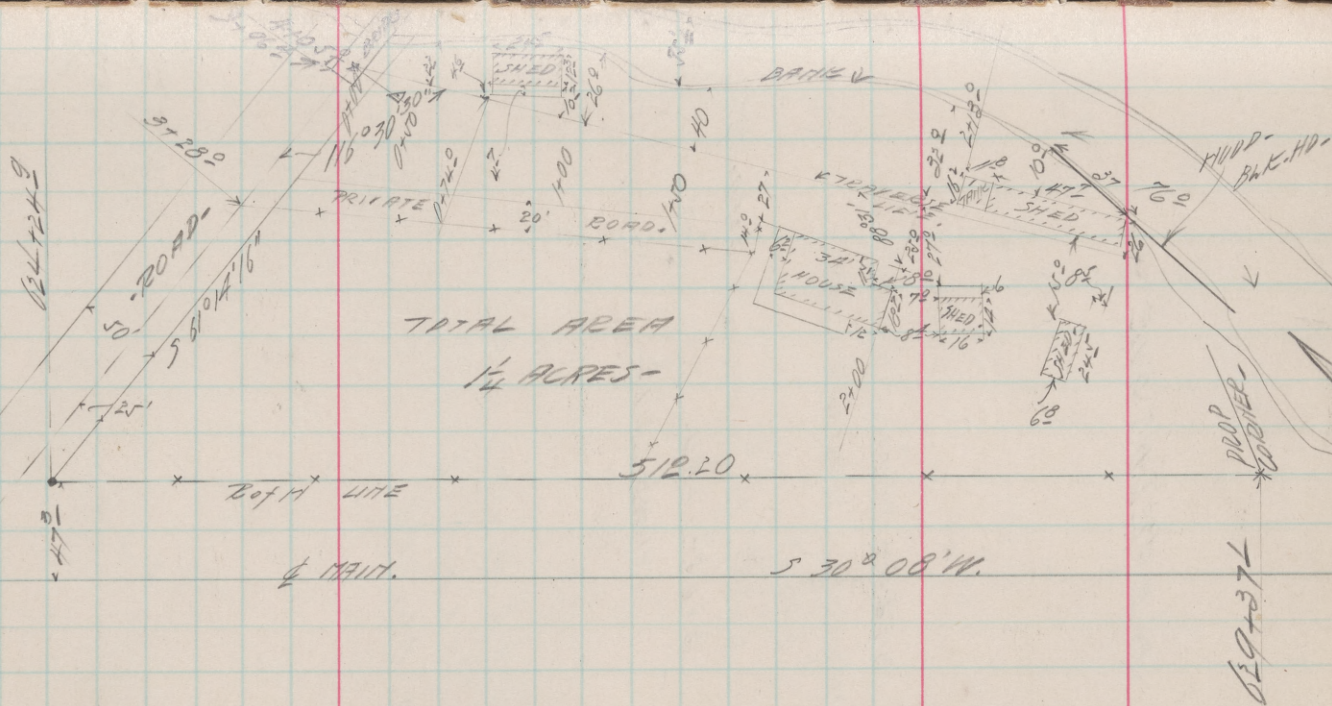
H. ANDREWS Rod.

G. BERRY -

0.2

CREEK

23x01-2



HEARLDSBURG.

to MILKITS-

P.S. 3538 + 787

2 + 234

2 + 834

2 + 452 END.

CENTERS. 276

LEAD- 787

75#

x 14109

- NO TIE PLATES-

P.F. #10. L.H.

S.T. 6D. RAIL.

60#

2 + 234

2 + 834 77

EC.

208

303

276

47

APRIL-8-'15.

CHECK SPUR TRACK
FOR SHELL OIL COMPANY.

3448

11-11-33 - 5.00 - 1.00

11-11-33 - 6.00 - 1.00

11-11-33 - 7.00 - 1.00

11-11-33 - 8.00 - 1.00

11-11-33 - 9.00 - 1.00

11-11-33 - 10.00 - 1.00

11-11-33 - 11.00 - 1.00

11-11-33 - 12.00 - 1.00

11-11-33 - 1.00 - 1.00

11-11-33 - 2.00 - 1.00

11-11-33 - 3.00 - 1.00

11-11-33 - 4.00 - 1.00

- HEALDSBURG -

P.S. 0+00-

LEAD-77⁶ RIGID-#9 60#

1+14⁵ END- 60#

1+88⁰ ϕ CGD 67A11

4+81⁰ ϕ WATER TANK ON RT. N⁴ from

ϕ 11⁶ 59.

OK 5+84⁰ 56# to 60#

✓ 5+96² P.S. P.F. #9. RIGID.

LEAD- 79⁸

9+15⁴ N. LINE BUNKERS-

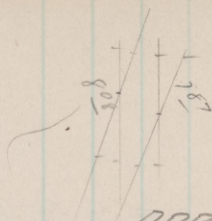
10+44² 56# to 60#

✓ 10+51³ P.S. 60# RIGID #9

11+33⁰ 60# to 56#

14+55² N.E. ROCK CRUSHER,

17+45⁵ END-



APRIL 8-15

Location of Tracks at Grant Gravel Spur

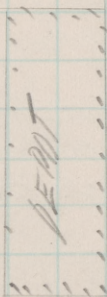
LENGTH. $6+61\frac{0}{2}$ { P.S. 0+00.
1+08' = 60# to 56#
5+16' = 56# to 50#

LENGTH. $1+39\frac{4}{2}$ { P.S. 0+00
0+98' = 60# to 56#
750' = LEAD. 60#
1+39' END.

- HEARLDSBURG -

LOCATION -

WATER CLMS -



13'

0
0

2642

to WHITES,

35

LARKSPUR

CREEK

4+20
4+00
3+50

3+36°

27°

3+00

2+70°

2+50

#1 - CREEK

2+10

2+10

2+50

2+100

2+50

2+50

E.B. MAINT - 2

TO MILLITS -

LOCATION OF CREEK
AT - 2-36" CONCRETE
PIPES -

LEVELS.

CITY BENCH
NAIL IN CONCRETE SIDEWALK
CORNER LOT #9, B&K H. - of TOWN
of LAKE SPUR.

STA. + X - Rod - Elev.

B.M. 2.25 28.09 25.84

BOT.

11/2 H PROP. -11.0 17.09
SOUTH LINE
17 AG. ST.

1/2 WAY BET. & DITCH -11.65 16.44
ABOVE & SPUR.

BOT. BOX-SPUR TRACK. -12.2 15.89

TOP RAIL SPUR. -9.95 18.14

T.P. -7.95 20.14 -

+2.04 23.08

-WEST CREEK.

PROP. LINE BOTTOM. -7.85 15.23
ON LEFT.

HT. B&K HD. -8.5 14.58

TOP RAIL E.B.M. & GUY -1.0 22.08

BOT. CREEK AT B&K HD. "BT" -9.0 14.08

DISTANCE FROM.

& E.B. MAINT. -9.5 13.78

-11.3 26.5 11.78

-10.6 12.48
62-

LEVELS - AT CREEK

AT BALLAST DECK -

LAKE SPUR.

11

STA.	+ X	-	ROD -	Elev.
	23.08		- 11.6 83.0	11.48
			- 12.2 117	10.88
			- 12.7 144	10.38
			- 14.2 165	8.88
			- 12.0 190	11.08
			- 11.9 250	11.18

STREAM - MUDS:

PT. FOR A-SECTION - BANK	126	-	2+50	12.48
PT. ON SIDE	" - 9.7		1750	13.38
BANK	" - 8.9		1700	14.18

X-SECTION - LOCATED -

STA. 1700.

12.48 3.0	8.48 0.0	12.50 3.0	RAISE SLIGHT
	2' WATER		
13.38 3.0	8.38 BOT. 3.8' WATER CREEK	13.38 3.0	
12.48 5.0	11.20 0.5' WATER CREEK	12.50 5.0	

(3)

LEVELS - AT -

CONCRETE PIPES -

STA.	+	X	-	ROD-	ELEV.
T.P.	1.22	⁴¹			20.14
		21.36			
PT. WHERE DITCH					
CUTS - UNDER FENCE			-7.3		14.06
BUT. PIPES. LEFT.			-8.10		13.26
AT ME. GROUND. "			-8.75		12.61
BUT. PIPE CT.			-9.0		12.36
G. GROUND -			-9.5		11.86
STA. 0+50			-9.6		11.76
1+00			9.65		11.71
1+50			9.50		11.86
2+00			10.0		11.36
2+50			-10.3		11.06
3+00			10.8		10.56
3+50			11.0		10.36

- LARK SPUR

- LAKESIDE -

APRIL-12-15

21.36
1.8
20.56

- Rod -

7 - SEC.

TOP BAK. E.B.M. of CORR. PIPE

18.34

= 20.56

LEFT.

2

R.T.

6.55

Level.

7.0

Level. 6.7

8.5

9.6

0.0

11.0

6.0

7.0

9.0

9.7

9.65

9.7

7.0

"

10.0

3.0

3.0

0.0

3.0

6.0

7.55

9.5

9.5

9.0

7.5

"

9.0

5.0

0.0

6.0

7.0

8.0

9.0

9.4

10.0

10.0

9.0

8.3

9.0

7.0

6.0

0.0

4.0

4.0

9.0

(38)

17AT-16-1916.

M.H.M. -

G.L.B. -

M.E. -

- LARKSPUR.

LEVELS ON SPUR

CITY DATUM.

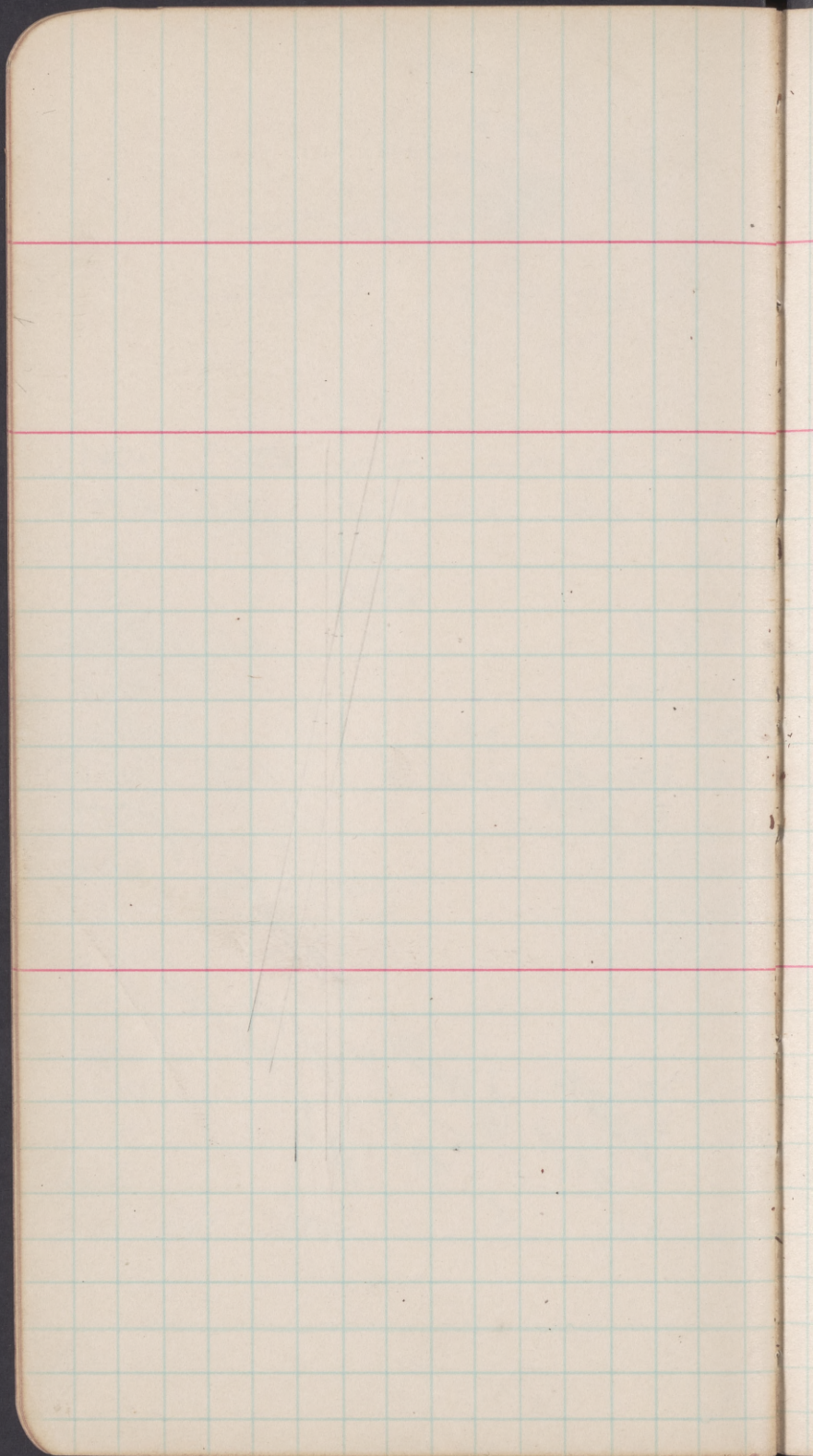
STA	+	✕	-	ROD ELEV
B.M.	0.96	26.80		25.84
T.P.				18.21
	4.79	23.00		
0+00 - P.S. WITCH				
3+00			4.65	18.35
4+00			4.62	18.38
4+50			4.88	18.12
5+10			4.93	18.07
5+60			4.86	18.14
6+01.8	int. of STREET + of SPUR		4.79	18.21
6+50			4.78	18.22
7+00	T.P.		4.21	18.79
	+7.4	26.19		
7+50			6.71	19.48
8+00			6.09	20.10
9+00			5.55	20.64
9+28	END - SPUR.		1.33	24.86

L.C. DOUGHERTY
 MNG.
 LARKSPUR
 LUT. CO

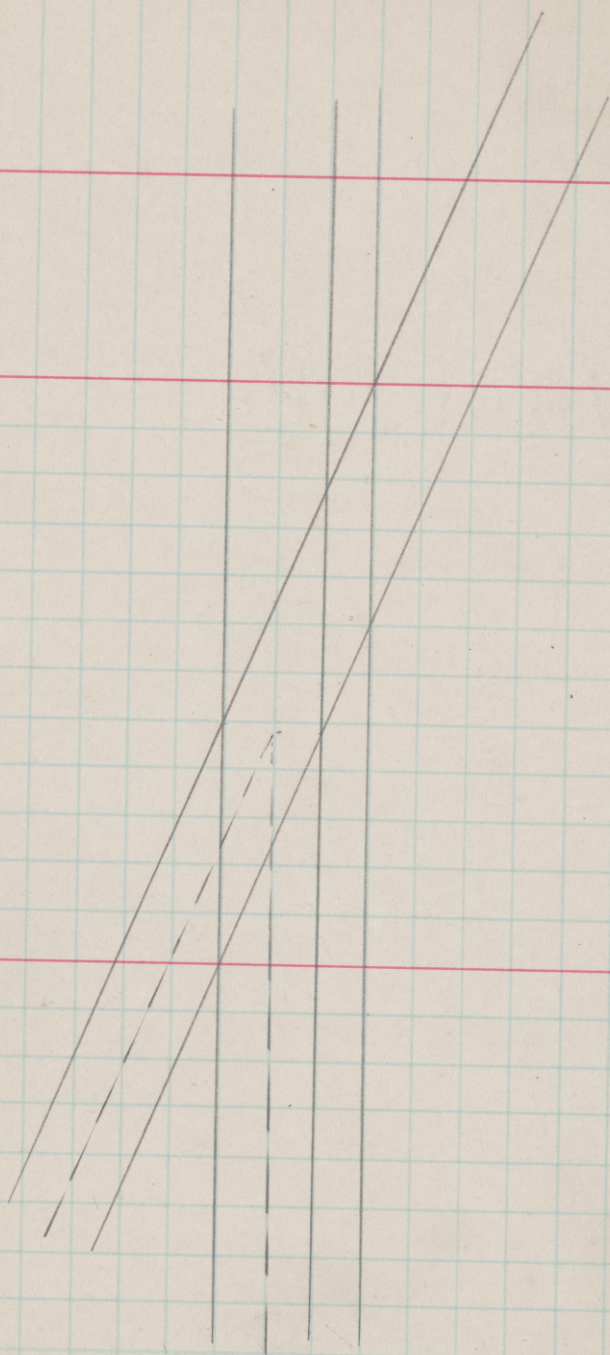
STA.	+	κ	-	Pod	ELEV
84	B.17.	0.58	26.42		25.84
21	=		8.21		18.21 ✓
			8.23		18.19
	6+01.8		-	8.2	18.22

235					
238	T.P.	+3.91	22.12		18.21
212	TOP RAIL	M.L. inter of ST	1.51		20.61
		M.B.			

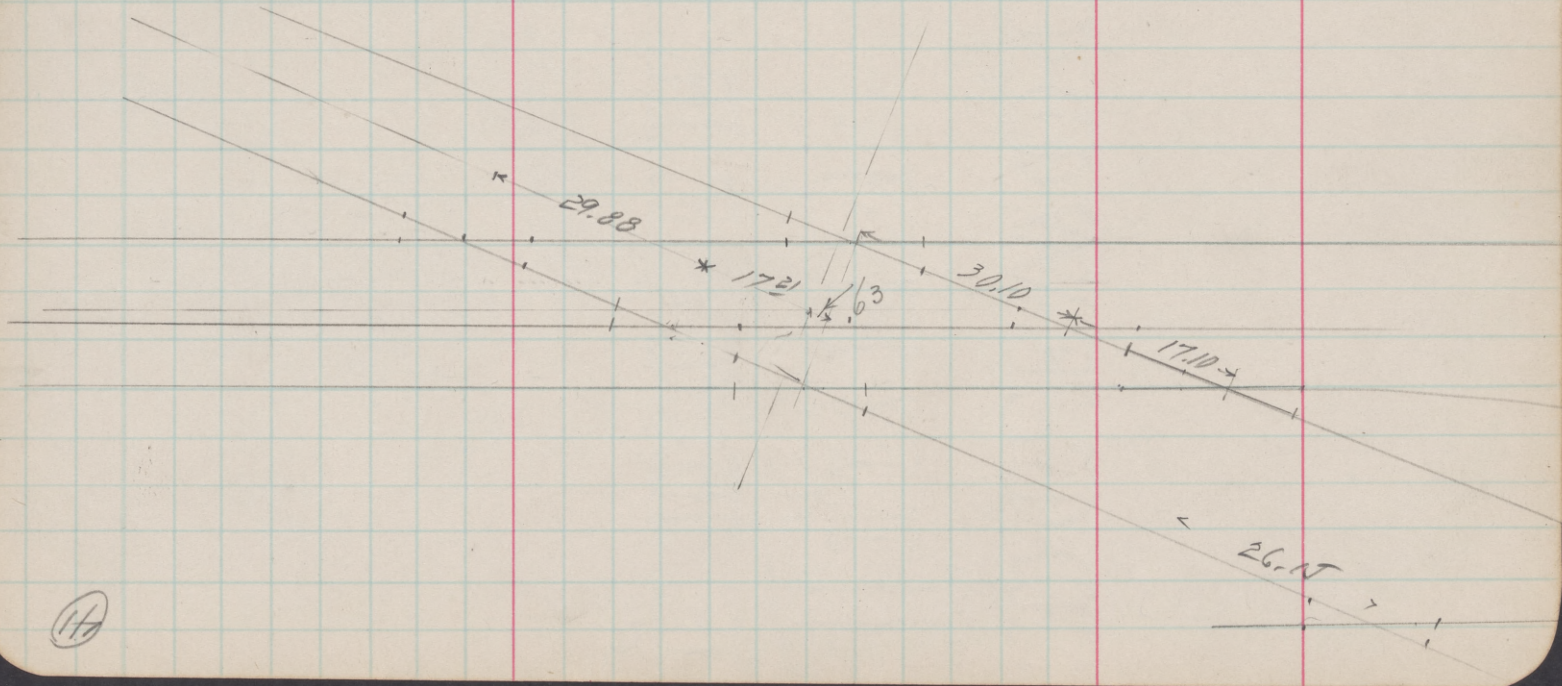
ELEV.
 Inter of WARD STREET
 & TOP RAIL
 W.B. TRACK

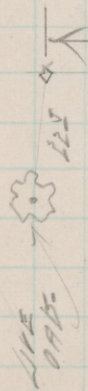


(40)



(14)





11th
0.95

125

329.6

578.87

"1590"

60.2

79.5

140 59'

137.70

291.74

"395.25"

63.0

180.28

196.72

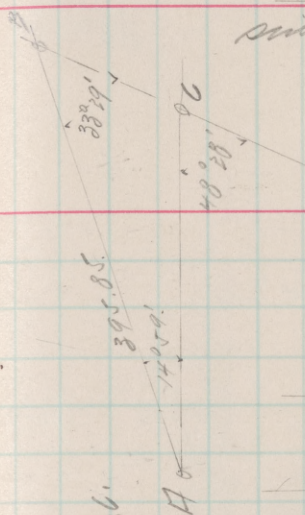
183.96

121.97

321.68

33°29'
145.59
48 28

$$\frac{395.85}{\sin 48^{\circ}28'} = \frac{BC}{\sin 145^{\circ}9'} = \frac{AC}{\sin 33^{\circ}29'}$$



$$\begin{aligned} &2.5975306 \\ &9.8742325 \\ &4.7232981 \\ &9.4125245 \\ &4.1358226 = \end{aligned}$$

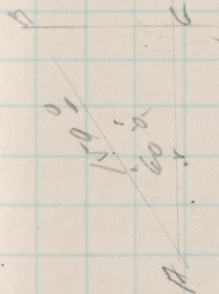
$$136.74 \text{ BC}$$

$$\begin{array}{r} 60.9 \\ 16.53 \\ \hline 77.43 \\ 730379 \\ \hline 48669 \\ 81.6 \\ \hline 13 \end{array}$$

$$\begin{aligned} &2.7232981 \\ &9.7416986 \\ &4.4649967 = \end{aligned}$$

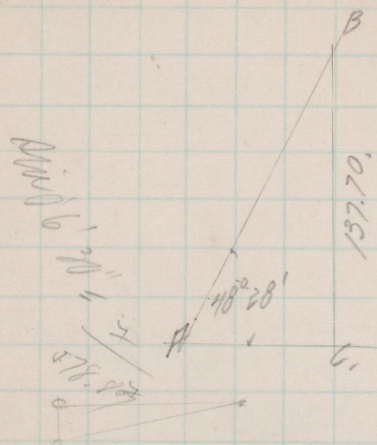
AC.

$$291.74$$



$$\begin{aligned} &\frac{150.5}{\sin 60^{\circ}} = \frac{BC}{\sin 159^{\circ}} \\ &\frac{150.5}{\sin 60^{\circ}} = \frac{AC}{\sin 159^{\circ}} \end{aligned}$$

$$\frac{150.5}{\sin 60^{\circ}} = 175.5$$



$$\begin{array}{r}
 2.1389339 \\
 9.8742325 \\
 \hline
 2.2649014 = 183.96 = AB
 \end{array}$$

$$\sin 48^{\circ} 28' = \frac{137.70}{AB}$$

$$\cos 48^{\circ} 28' = \frac{AC}{AB}$$

$$\cot F = 48^{\circ} 28' = \frac{AC}{137.70}$$

$$\begin{array}{r}
 .74857 \overline{) 137.70000} \\
 \underline{74857} \\
 3
 \end{array}
 \quad (1)$$

$$\begin{array}{r}
 578.87 \\
 320.983 \\
 \hline
 1099.853
 \end{array}$$

$$\begin{array}{r}
 .88576 \\
 137.7 \\
 \hline
 620032 \\
 620032 \\
 \hline
 265728 \\
 88576 \\
 \hline
 121.969152
 \end{array}$$

$$\begin{array}{r}
 186.72 \\
 183.96 \\
 \hline
 320.68
 \end{array}$$

$$\begin{array}{r}
 291.74 \\
 121.97 \\
 \hline
 169.77 \\
 79.50 \\
 \hline
 249.27 \\
 329.60 \\
 \hline
 578.87
 \end{array}$$

to party 200-

$$2009 + 88 \underline{46}$$
$$6 + 24 = 30$$

845 61.

124

281

570.87

24568

820.68

9745

✓ 0-100

96

-135

1103E

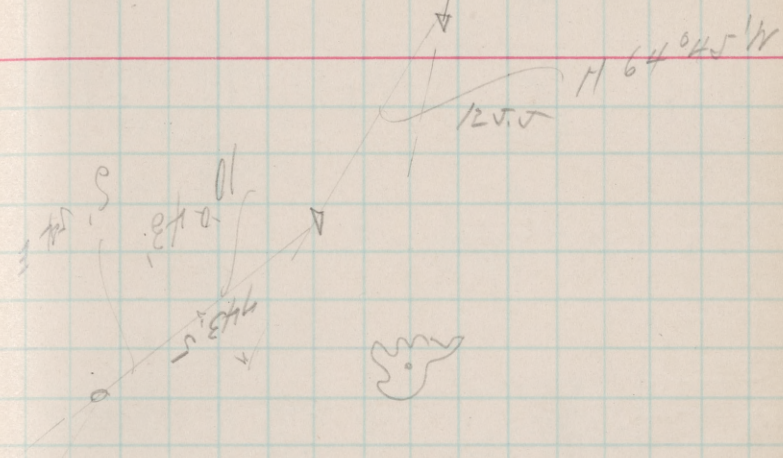
(43)

10/10

10/10

$$\begin{array}{r} 64 \\ 50 \\ 114 \\ 115 \end{array} \begin{array}{r} 27 \\ 102 \\ 42 \end{array}$$

$$\begin{array}{r} 179 \\ 115 \\ 64 \end{array} \begin{array}{r} 60 \\ 42 \\ 18 \end{array}$$



TIER "B"
MESA GRANDE

MESA GRANDE

1712

870330

7

174³

20

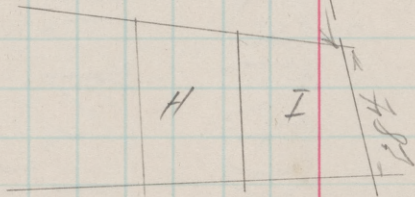
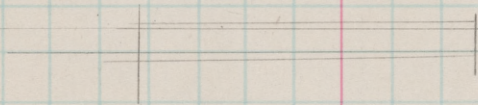
337⁴

Be over

74K

TRAVEL -

- MESA GRANDE -

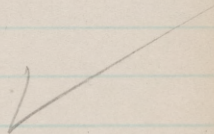


25
78

66

55.2760 + 0.6 =

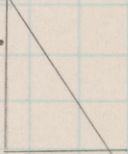
TO DUTCHMAN



(45)

2755+167

35°



28°33'

25

25

14.111T.
2756+283

56+602

TRETTLE-

74H.

15

15
35

ROAD.

CHIFFES.

2757+006

TO BUTCHART-



MESA GRANDE

WADSWORTH
CROSS

E.S. $2742 \pm 18'$

TO

DUTCHMAN'S

$2417 \pm$
 $42'$

304 I

LOT 58

0.700

BROADWAY AVE. 60'

E.S.

483

MONTTE RID-
-TIER B.

LOT.
90.

50°

TO FULTON

Φ NARROW
GAGE

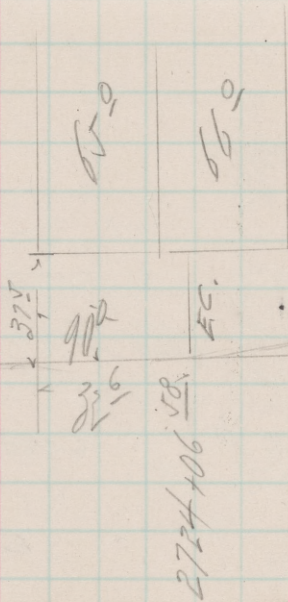
427.95

TO DUNCAN.



TIER "B"

MORTE RIO



46

TIER "B"
MONTE RIO

LOT 58-
N 52° 42' W

CASCADE LAKE

97° 25'

40' 1"

3 2/5' CURVE

256 1/2

R 72° 44' 0"

- CASCADE LAKE

TO MICHIGAN

CC 12th RT.
2713+029

2711+790

250

90th

LOT-11-

TIER A-

WHITE RIO

2711+790

LOT.

37.

LONG

6'

90°

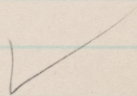
90°

29°

27/1/44

TIER "B"

TO DUNCATS



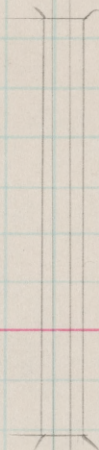
66

73 H.

8+436

27087566

2



TIER B-
MOUNTED R.D.

W.T.B.

2.6
3
30
29

10' LAKE

TO DUNCAN -

TIER "B"

LOT. 22 ✓

LOT. 23.

LAKE.

21'0"

10'0"

20'3"

75'2 1/2"

485

734

TO DUNCAN

✓
1043+430
905

1048+34
982

MORTE RIO.

TIER B

LOT. 1

LOT. 2

55°

89.0

101

33.9

1041+34.7

EC. - 1041+450

P.S. 1

TO PULCATH -

(50)

✓
33.9
101
35

LOT. 1.

LOT. 2.

TIER
- A.

90°
90°
↓

MOTTE RID.

TO DUNGHAN.

MRIH.

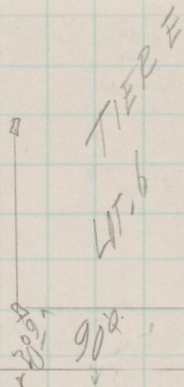
to Pt. 54. 2716 →

ABOUT
PT. REVERSE

(57)

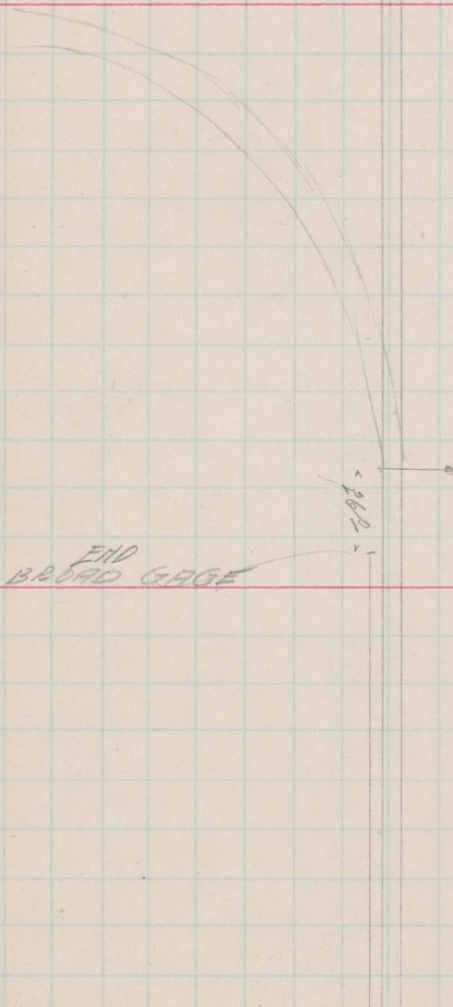
374.6
- 2.93

371.67



PULCH

MILLS



$$\begin{array}{r} 200 \\ 100 \\ 600 \\ 200 \\ \hline 900 \end{array}$$

To Mark

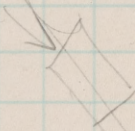
Monte Rio
 504' west
 west 2W

00+0

340

$$\begin{array}{r} 1033 \\ 20 \\ 15 \\ 990 \\ 30 \\ \hline 33 \end{array}$$

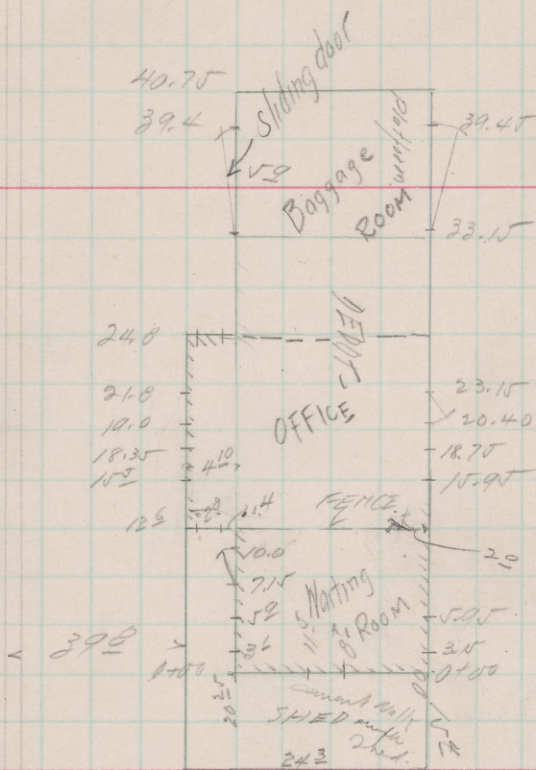
$$\begin{array}{r} 200 \\ 100 \\ 20 \\ \hline 320 \end{array}$$



20+6

10+33

57



Ponchaux Mills Depot.

TO ADRIE BO-

53

BUT. PIDE LEFT.	9.85	
" " H.	10.45	ETCH
top rail.	104.3	
BOT. 9d. under bridge	9.75	ht
" " " "	8.64	R 9.57
then - 1+00.	8.5	
2+00	8.6	95.7

T.P.	7.9	+ 4.0	H.I. 100.4	96.4
3+00.			-5.0	95.4
4+00			-5.0	
5+00			-5.6	
6+00	+6.1	H.I. 101.0	-5.5	94.9
7+00			-6.1	
8+00			-6.2	
9+00			-6.2	
10+00			-6.3	94.5

1400 UP. CREEK. distance. 7.6

2100 7.1

3100- 6.2

4100- 6.2

5100 6.0-

top road- 5.4

- GETTERVILLE-

Prop. lowering of Calvert

PARKINSON

520

53

279
525x0
12x2
16
92
2x072
2x072

BRIDGE

2x77x30

20x10

2x54

2x50

2x00x13

1x70

59x34

72x100

2x81.4x3

0x50

3x041

0x00

32

1x192

CEMENT SIDE MARK

3RD ST.

60'

400-

MAIN

179.64
120.34
59.30

8' PLAT

PLAT

2x072

1400

8105 - 07.166

1200

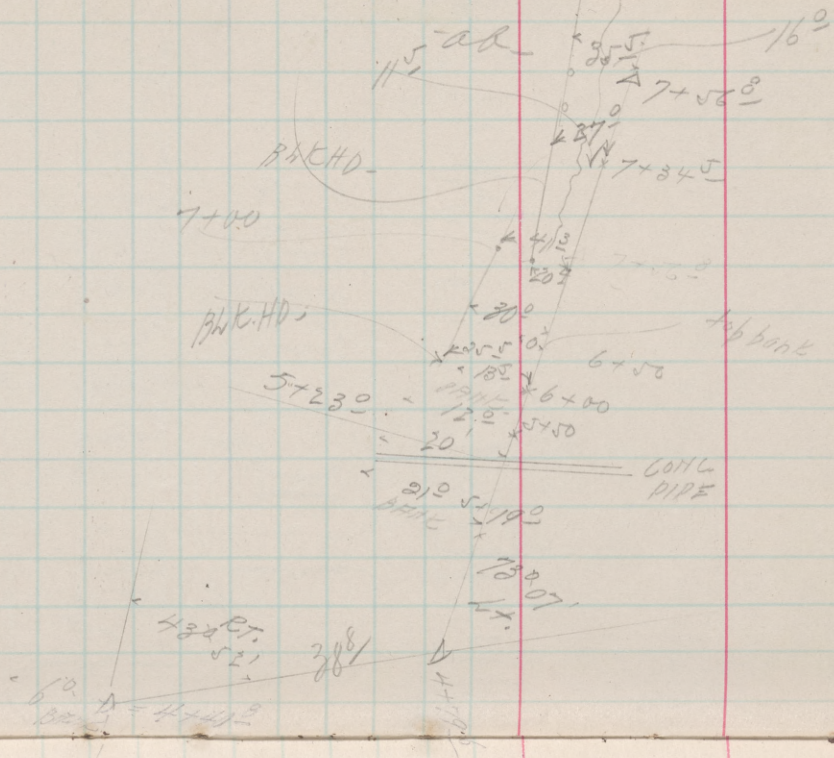
1200

1200

1200

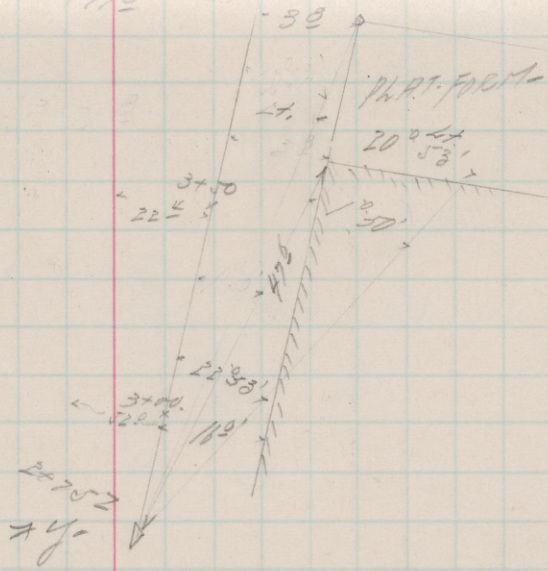
1200

$$\begin{array}{r}
 7+56^8 \\
 4+79^6 \\
 \hline
 2 \quad 77^{\frac{2}{2}}
 \end{array}$$



3+77.8

3+77.8



$$\begin{array}{r} 4+40.8 \\ 2+15.7 \\ \hline 65.5 \end{array}$$

$$\begin{array}{r} 7+56.8 \\ 4+79.6 \\ \hline 277.2 \end{array}$$

79

Concrete
matt 10' x 96'

11x29

114389

PL. M. B. 100

235

 $\frac{1}{\sqrt{2}}$

$9+63^{\circ}$ ANGLE.

ANGLE-

16th - 80th / 50th 1st

END. BAK. 10.16.00
10.16.00
10.16.00

22⁰ 54

 ≈ 12.4

ON BANK
9 + 50°

← 209

 $\frac{1}{6}$

9-29-3

54 57
36° 45'
18° 12'

32' 254'

$$\begin{array}{r} 18^{\circ} 12' \\ 14^{\circ} 50' \\ \hline 33^{\circ} 02' \end{array}$$
$$\begin{array}{r} 9 + 28 \\ 7 + 56 \\ \hline 171 \end{array}$$

82 3/28/11
53

54th. 57th
Lt.

26 45' Lt.

ВЗРК.

"AB"

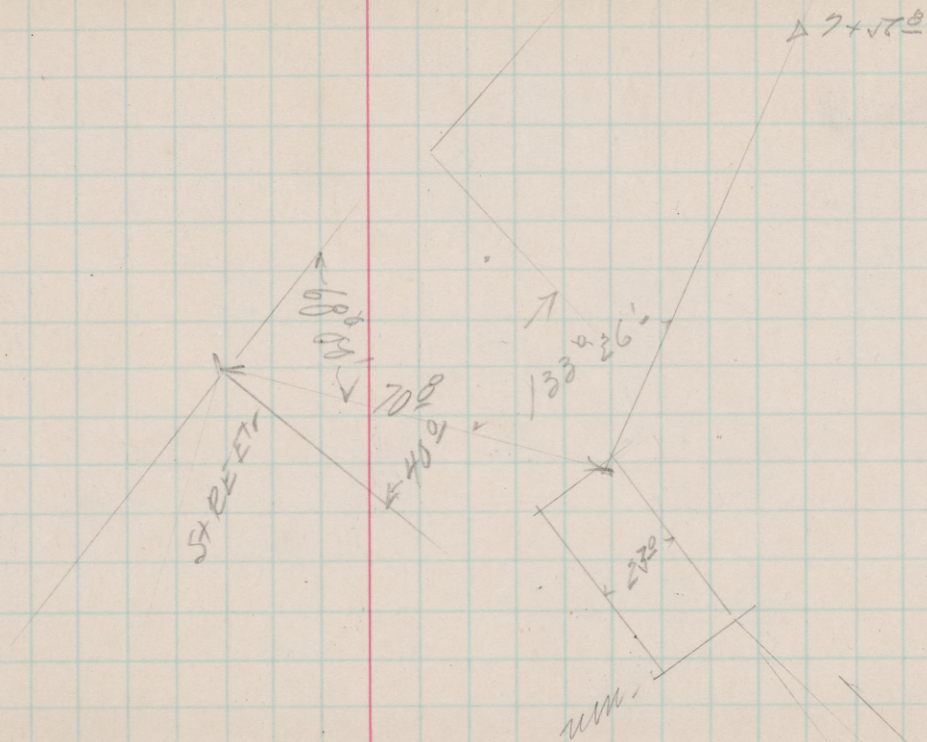
$$7 + \sqrt{6} - 8$$

14.51

JK 57

$$\begin{array}{r} 89 \text{ } 60 \\ 80 \text{ } 42 \text{ } 1 \\ \hline 90 \text{ } 18 \end{array}$$

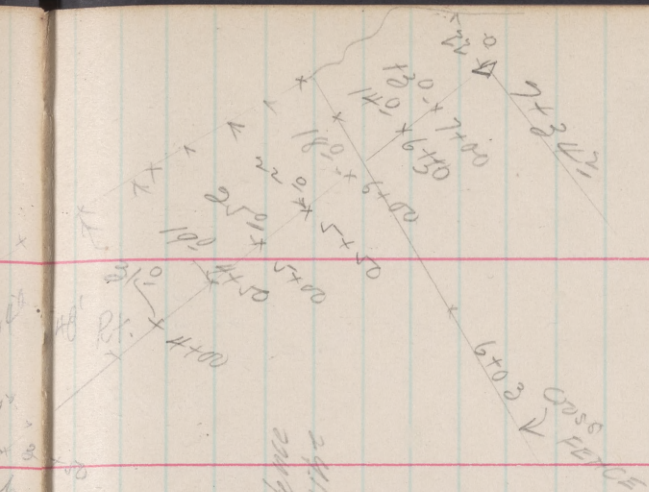
(25)



PROP. LINE
N^o 2

300'

19.00



Job high
BANK on fence

92.27

0+00

ACIDGE

$$\begin{array}{r} 3+15.6 \\ 2+03.6 \\ \hline 1+12.0 \end{array}$$

25.4

H. beqni

1.22 0.25

11+10.5

BRIDGE

48.03' Lt.

19+86.4

11+84.5

77.04' Lt.

50'

8+10

240

8.54' Lt.

9+09.5

7+34.5

1.20 0.25

11+30.4

1.20 0.25

$$\begin{array}{r} 10 + \\ 9 + 86 \end{array} \quad \underline{\quad} \quad \text{S}$$

$$\begin{array}{r} 10 + 849 \\ 9 + 86 \end{array} \quad \underline{\quad} \quad \text{S}$$

$$\underline{\quad} \quad 985$$

14+05? Opp. Pt. Passing off R. of W. Line

- WILLITS -

Proposed Spur to Serve
Standard Oil Company -

10-21-1915 W.T.R.

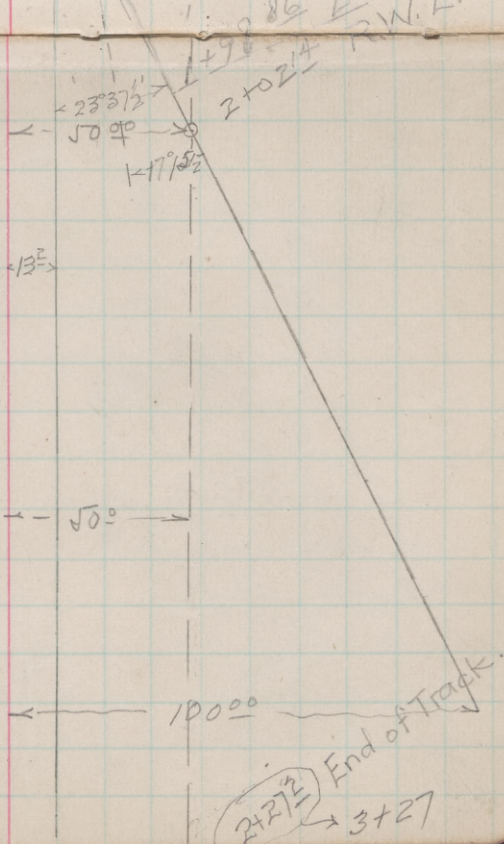
S.M.J. Andrews -
G.L. Berry -

12+91 $\frac{1}{2}$ Opp. Prop. End of Spur -

Storage

Willits & Burr Spur = 626' Length -

To Willits Depot



18+08⁰ P.S. Willis & Burr Spur

17+27⁵ P.F. #9

16+12⁹ P.S. Storage Track

16+02⁸ P.S. Prop. Std Oil Spur = 2+05⁸ Spur

16+00³ Change in Steel Spur 2+08⁴ Spur Rail $\frac{65\#}{56\#}$

15+71⁹ Opp. P.I. #9 Turnout

15+29¹ Opp. Prop. P.F.

15+19¹ " B.C.

14+61⁷ Opp. P.I. 15° Curve

MAIN

To Sherwood

(62)

0+00

← 50° →

$\frac{2+05^8}{0+00} =$

P.S.

0+00

0+31⁰ Δ P

0+73⁸ P.F. #9

0+83⁸ B.C. 15° Lt

→ 6° 22'

125-48

86 E.C.
+98
214 R.W. Line

+35
+50
+65

45 96.2
51 96.0

377 97.35

2

+25

+50

+65

Grade
rods.

94.3
96.5
2.2

342

342

55

95.6

X

450

96.62

96.37

PHATT. Bldg.
0.33

55

95.6

60

95.1

450

96.62

62

94.9

Level

3

+27.2

345

356

53

95.8

450

96.52

345

353

54

95.7

450

96.52

96.35

WILLIS -
Elevations & Grades Over
Prop. Spur To Serve
Standard Oil Co.

10-21-15 W.T.R. / M.A.
G.L.B.

Station + H.I. - Elev. - Top of Rail Grade -
 B.M. 100.00 B.M. - Track Spike In Oak 100' R 14 + 50

$\sqrt{54}$ 112 101 $\frac{1}{2}$

0 + 00	H.I. 99.78	99.3	
0 + 73.8	29	98.3	
0 + 80	31	98.0	2.65
0 + 83.8	35	97.6	2.94
1	45	96.9	

ACTUAL BODS. -
 100' R 14 + 50

Top of Tie - May Be
 Yardage Estimate Prepared On Basis Of Ground
 Being Entirely Level.

+35
 +50

377 97.35

16+69[±] Line of Paving.

MAIN

16+44[±] Line of Paving On Main Line.

+2°-->

238

224

Bitumen Pavement

240

West Prop. Line

1+438 Line of Paving

1+69° Line of Paving
ST.

--2°-->

East Prop. Line

← To Road

- WILLITS -

- Area Of Main St. Roadway -

Bitumened By R.R.

N.T.R. J.W.J.A.
G.L.B.

18+08 = P.S. Willits & Burr Spur -

552 Sq. Feet
of Bitumen -

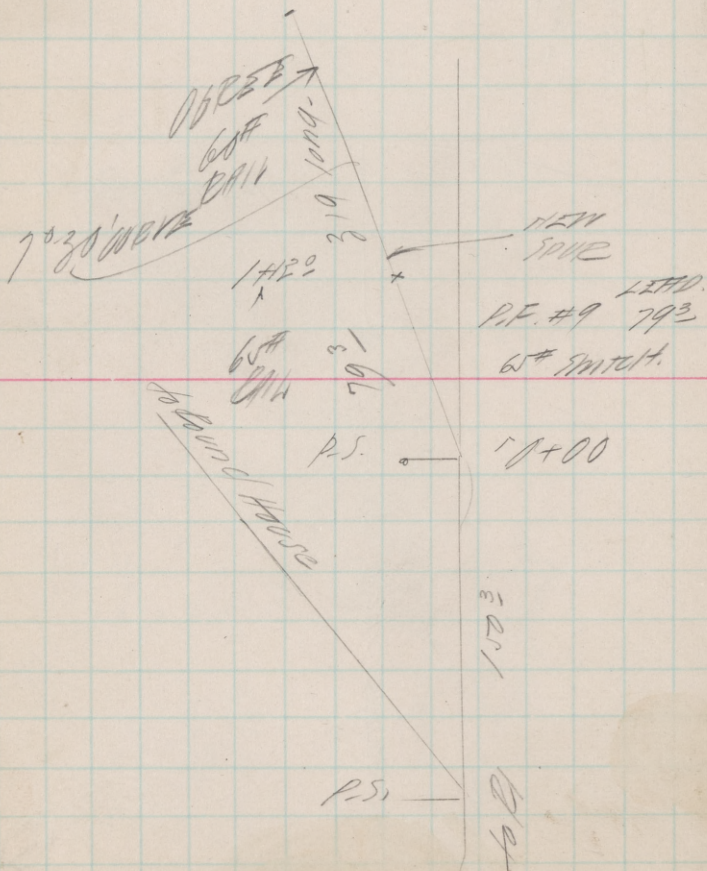
17+27 $\frac{1}{2}$ R.F. #9 Fig

To Sherwood →

0+00 Spur Stationing

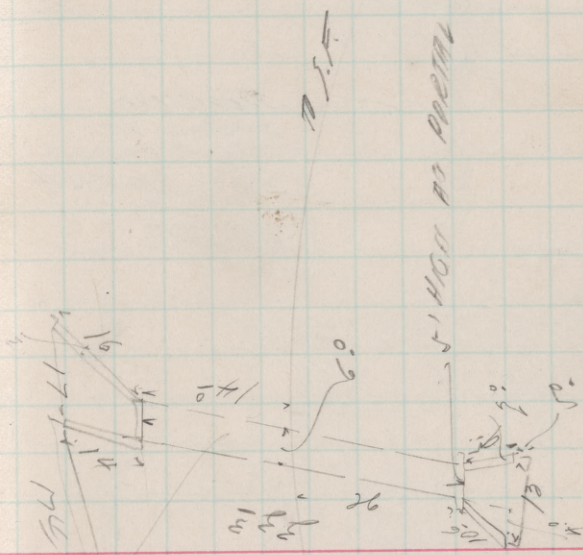
(63)

- MILLITS -
 LOCATION NEW STORAGE
 TRACK FOR ENGINES.



WEST OF RIDGEWOOD.

LOCATION
CONCRETE ARCH



3/9
7/9
0/8
3

— RIDGEWOOD —

LOCATION NEW.

— WOOD SHEDS —

LINE TO S.F.

LOCATION
SHOWN ON
PREVIOUS
SKETCH.

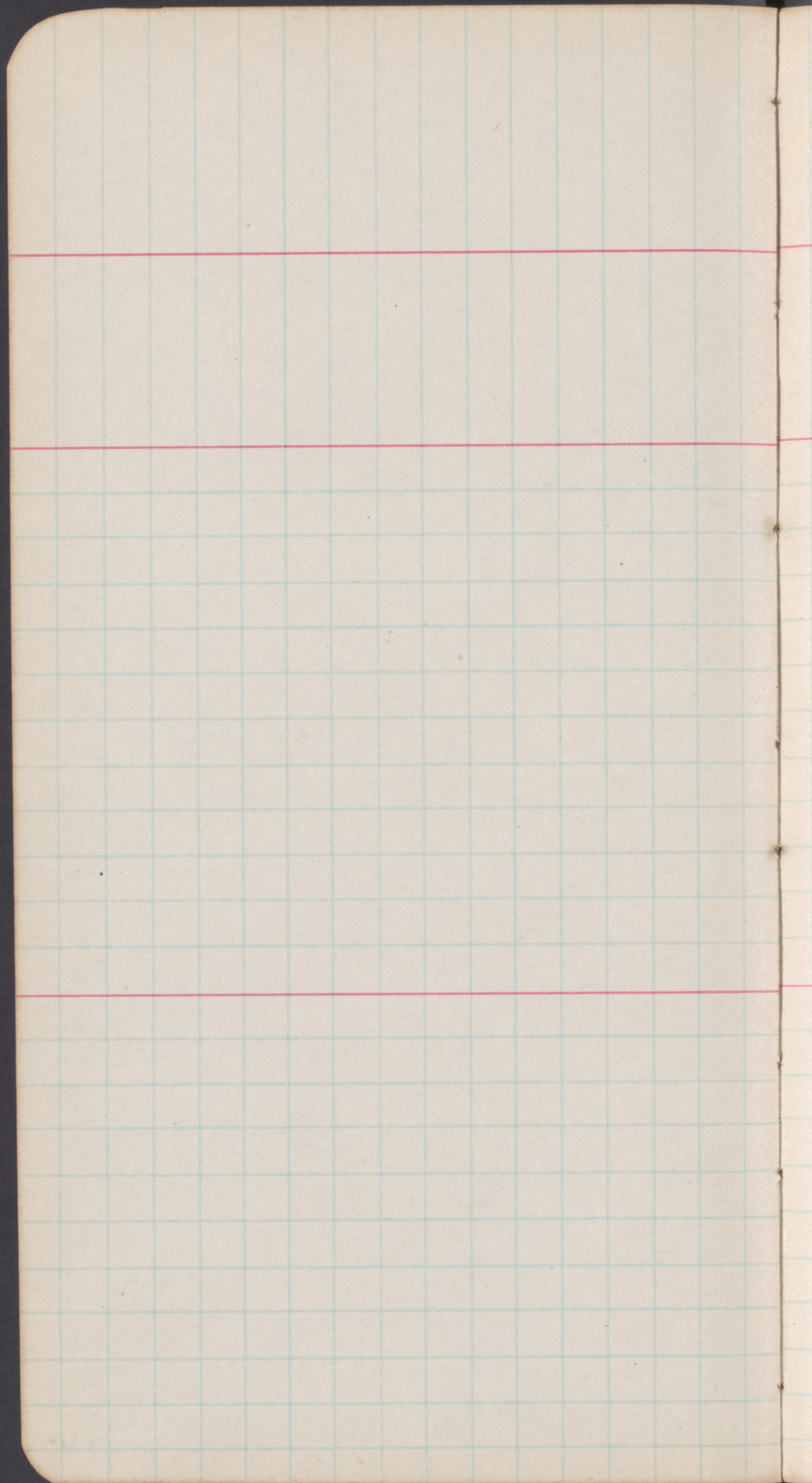
WOOD SHED.

BUNK
HOUSE

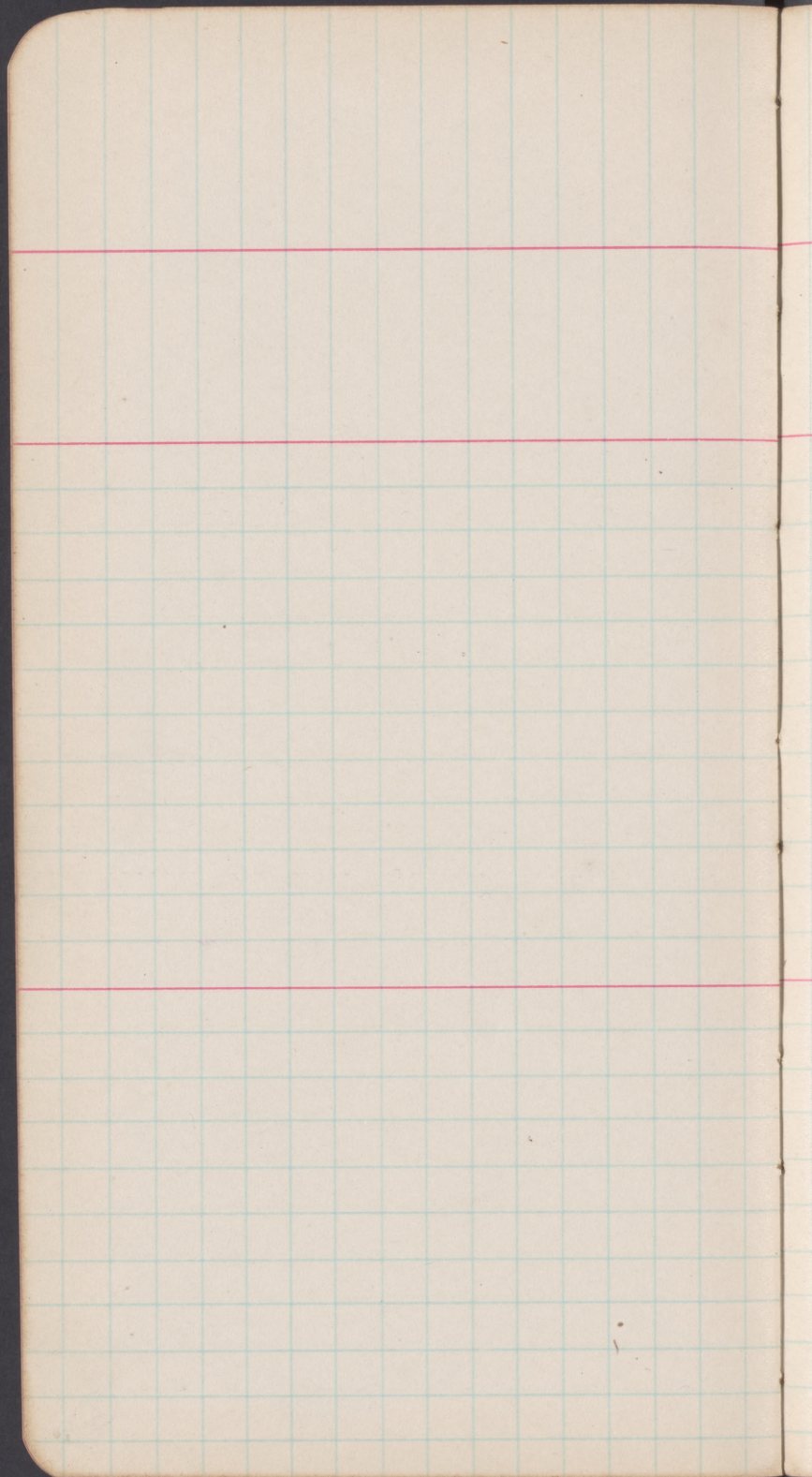
WOOD SHED.
10' x 10'
10' x 10'
10' x 10'

13' x 7' long
extend 14' west

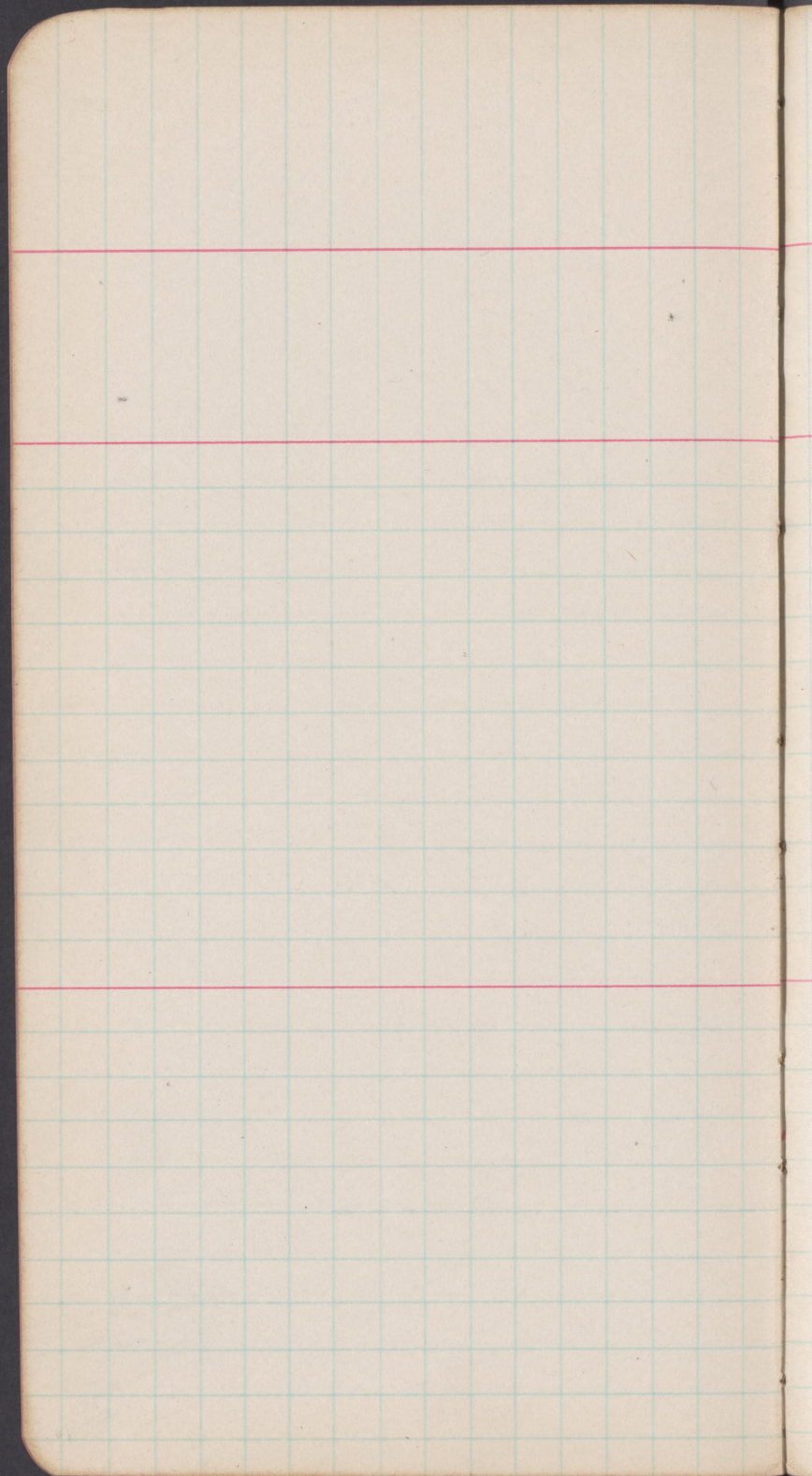
65



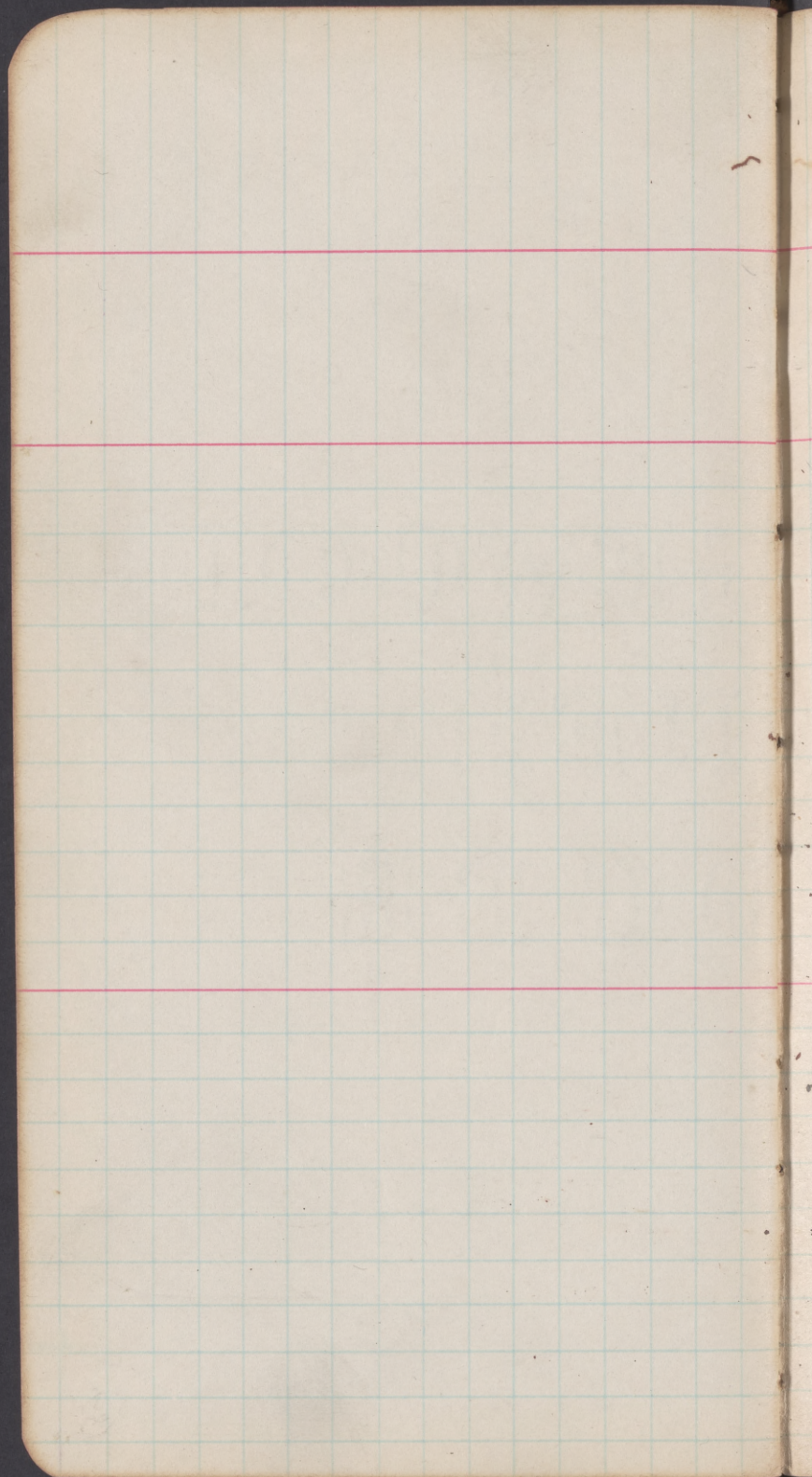
66



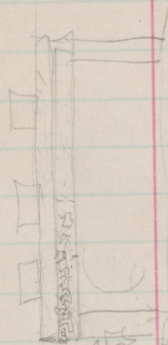
(67)



(68)

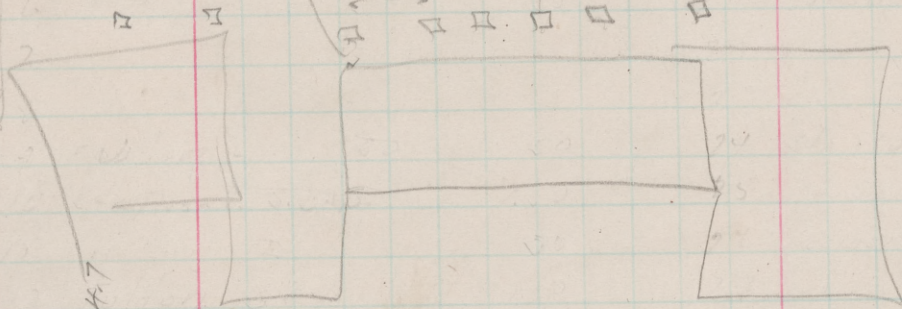


(69)



1700

4.7



1000

1000

1000

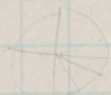
5000

5000

$$\begin{array}{r} 109 \\ 3.3 \\ \hline 42 \end{array}$$

S 69° 47' E

S' 53° 37' E



5-5-

$$\begin{array}{r} 357 \\ 38.85 \\ \hline 85 \end{array}$$

$$\begin{array}{r} +3 \\ 5.5 \\ \hline 8.5 \end{array}$$

6.

$$\begin{array}{r} 6.0 \\ 4.8 \\ \hline 1.2 \end{array}$$

H1- 1+

$$\begin{array}{r} 4.2 \\ 1.6 \\ \hline 2.6 \end{array}$$

1-6.

$$\begin{array}{r} 5.0 \\ 1.6 \\ \hline 3.4 \end{array}$$

16°

$$\begin{array}{r}
 156.25 \\
 16 \overline{) 25} \\
 \underline{16} \\
 90 \\
 \underline{80} \\
 100
 \end{array}$$

Pearl 196 Rankin
 Mrs. W. Moore
 Mrs. 86. W. Betray

$$\begin{array}{r}
 81 \\
 250 \\
 \underline{3} \\
 3775
 \end{array}
 \quad
 \begin{array}{r}
 78 \\
 1 \\
 796
 \end{array}
 \quad
 \begin{array}{r}
 33 \\
 17 \\
 \underline{1.6} \\
 78 \\
 796
 \end{array}$$

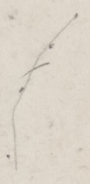
62.

357

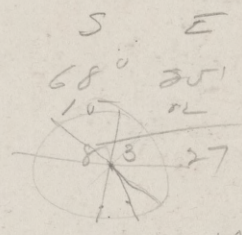
$$\begin{array}{r}
 7 \\
 91 \\
 \underline{2} \\
 101
 \end{array}$$

$$\begin{array}{r}
 17 \\
 52 \\
 91 \\
 8
 \end{array}$$

$$\begin{array}{r} 60 \\ 45 \ 02 \\ \hline 15 \ 02 \end{array}$$



$$\begin{array}{r} 633+082 \\ 8+883 \\ \hline 24+24 \end{array}$$

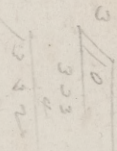


$$\begin{array}{r} 2+554 \\ 713 \\ \hline \end{array}$$

$$3+267$$

$$1.0.6$$

$$\begin{array}{r} 481.3 \\ 402.0 \\ \hline 883.3 \end{array}$$



$$\begin{array}{r} 6+61 \\ 5+53 \\ \hline 1108 \end{array}$$

$$\begin{array}{r} 6+61 \\ 0+45 \\ \hline 5+16 \end{array}$$

